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Vanadium (beta-(dimethylamino)ethyl)cyclopentadienyl complexes with diphenylacetylene ligands

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Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F , and R-factors based on ALL data will be even larger.

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 H6B H Uiso -0.20743 0.13511 0.37619 1.000 0.0250 . .
 H7A H Uiso -0.32420 0.09055 0.17883 1.000 0.0242 . .
 H7B H Uiso -0.31492 0.12742 0.07517 1.000 0.0242 . .
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 H8B H Uiso -0.04170 0.05645 0.06932 1.000 0.0292 . .
 H8C H Uiso -0.19387 0.08493 -0.02327 1.000 0.0292 . .
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 H9B H Uiso 0.05750 0.05496 0.32789 1.000 0.0302 . .
 H9C H Uiso -0.11478 0.04743 0.31494 1.000 0.0302 . .
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 H13 H Uiso 0.75806 0.17699 0.66674 1.000 0.0230 . .
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 C3 0.024(3) 0.012(2) 0.025(2) -0.0006(19) 0.017(2) 0.0010(19)
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 from the variances of the (full) variance-covariance matrix.
 The cell esds are taken into account in the estimation of
 distances, angles and torsion angles

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C6	H6A	0.9900	. .	no
C6	H6B	0.9900	. .	no
C7	H7A	0.9900	. .	no
C7	H7B	0.9900	. .	no
C8	H8A	0.9800	. .	no
C8	H8B	0.9800	. .	no
C8	H8C	0.9800	. .	no
C9	H9A	0.9800	. .	no
C9	H9B	0.9800	. .	no
C9	H9C	0.9800	. .	no
C12	H12	0.9500	. .	no
C13	H13	0.9500	. .	no
C14	H14	0.9500	. .	no
C15	H15	0.9500	. .	no
C16	H16	0.9500	. .	no
C19	H19	0.9500	. .	no

C20	H20	0.9500	. .	no
C21	H21	0.9500	. .	no
C22	H22	0.9500	. .	no
C23	H23	0.9500	. .	no
C26	H26	0.9500	. .	no
C27	H27	0.9500	. .	no
C28	H28	0.9500	. .	no
C29	H29	0.9500	. .	no
C30	H30	0.9500	. .	no
C33	H33	0.9500	. .	no
C34	H34	0.9500	. .	no
C35	H35	0.9500	. .	no
C36	H36	0.9500	. .	no
C37	H37	0.9500	. .	no

loop_

_geom_angle_atom_site_label_1

_geom_angle_atom_site_label_2

_geom_angle_atom_site_label_3

_geom_angle

_geom_angle_site_symmetry_1

_geom_angle_site_symmetry_2

_geom_angle_site_symmetry_3

_geom_angle_publ_flag

N	V	C1	96.63 (14)	.	.	.	yes
N	V	C2	131.79 (16)	.	.	.	yes
N	V	C3	131.01 (16)	.	.	.	yes
N	V	C4	95.24 (15)	.	.	.	yes
N	V	C5	75.68 (15)	.	.	.	yes
N	V	C10	112.60 (15)	.	.	.	yes
N	V	C17	96.71 (15)	.	.	.	yes
N	V	C24	97.61 (14)	.	.	.	yes
N	V	C31	116.32 (15)	.	.	.	yes
C1	V	C2	35.69 (16)	.	.	.	yes
C1	V	C3	59.78 (14)	.	.	.	yes
C1	V	C4	60.18 (14)	.	.	.	yes
C1	V	C5	36.04 (16)	.	.	.	yes
C1	V	C10	90.56 (17)	.	.	.	yes
C1	V	C17	126.97 (15)	.	.	.	yes
C1	V	C24	158.56 (16)	.	.	.	yes
C1	V	C31	142.41 (15)	.	.	.	yes
C2	V	C3	35.78 (14)	.	.	.	yes
C2	V	C4	59.94 (15)	.	.	.	yes
C2	V	C5	59.89 (17)	.	.	.	yes
C2	V	C10	82.33 (16)	.	.	.	yes
C2	V	C17	116.72 (16)	.	.	.	yes
C2	V	C24	129.88 (17)	.	.	.	yes
C2	V	C31	107.91 (16)	.	.	.	yes
C3	V	C4	36.08 (17)	.	.	.	yes
C3	V	C5	60.20 (16)	.	.	.	yes
C3	V	C10	110.03 (16)	.	.	.	yes
C3	V	C17	132.16 (17)	.	.	.	yes
C3	V	C24	119.55 (16)	.	.	.	yes
C3	V	C31	84.09 (16)	.	.	.	yes
C4	V	C5	36.40 (15)	.	.	.	yes
C4	V	C10	142.24 (16)	.	.	.	yes
C4	V	C17	165.01 (16)	.	.	.	yes
C4	V	C24	133.82 (14)	.	.	.	yes
C4	V	C31	97.30 (17)	.	.	.	yes
C5	V	C10	125.56 (16)	.	.	.	yes
C5	V	C17	157.20 (14)	.	.	.	yes

C5	V	C24	165.16 (15)	.	.	.	yes
C5	V	C31	133.49 (17)	.	.	.	yes
C10	V	C17	37.40 (15)	.	.	.	yes
C10	V	C24	69.17 (16)	.	.	.	yes
C10	V	C31	92.7 (2)	.	.	.	yes
C17	V	C24	35.11 (14)	.	.	.	yes
C17	V	C31	69.22 (17)	.	.	.	yes
C24	V	C31	37.91 (16)	.	.	.	yes
V	N	C7	110.0 (2)	.	.	.	yes
V	N	C8	116.3 (3)	.	.	.	yes
V	N	C9	107.1 (3)	.	.	.	yes
C7	N	C8	106.3 (3)	.	.	.	yes
C7	N	C9	108.6 (3)	.	.	.	yes
C8	N	C9	108.4 (3)	.	.	.	yes
V	C1	C2	71.6 (2)	.	.	.	yes
V	C1	C5	70.9 (2)	.	.	.	yes
C2	C1	C5	107.6 (3)	.	.	.	no
V	C2	C1	72.7 (2)	.	.	.	yes
V	C2	C3	71.8 (2)	.	.	.	yes
C1	C2	C3	108.7 (4)	.	.	.	no
V	C3	C2	72.5 (2)	.	.	.	yes
V	C3	C4	71.6 (2)	.	.	.	yes
C2	C3	C4	108.1 (4)	.	.	.	no
V	C4	C3	72.3 (3)	.	.	.	yes
V	C4	C5	72.0 (3)	.	.	.	yes
C3	C4	C5	107.7 (4)	.	.	.	no
V	C5	C1	73.1 (3)	.	.	.	yes
V	C5	C4	71.7 (3)	.	.	.	yes
V	C5	C6	115.5 (3)	.	.	.	yes
C1	C5	C4	107.9 (4)	.	.	.	no
C1	C5	C6	125.8 (4)	.	.	.	no
C4	C5	C6	125.9 (4)	.	.	.	no
C5	C6	C7	108.1 (4)	.	.	.	no
N	C7	C6	111.5 (4)	.	.	.	yes
V	C10	C11	142.6 (3)	.	.	.	yes
V	C10	C17	89.5 (3)	.	.	.	yes
C11	C10	C17	127.6 (4)	.	.	.	no
C10	C11	C12	119.7 (4)	.	.	.	no
C10	C11	C16	122.9 (4)	.	.	.	no
C12	C11	C16	117.4 (4)	.	.	.	no
C11	C12	C13	121.4 (4)	.	.	.	no
C12	C13	C14	119.5 (5)	.	.	.	no
C13	C14	C15	120.2 (4)	.	.	.	no
C14	C15	C16	120.5 (4)	.	.	.	no
C11	C16	C15	121.0 (4)	.	.	.	no
V	C17	C10	53.1 (2)	.	.	.	yes
V	C17	C18	146.0 (3)	.	.	.	yes
V	C17	C24	71.6 (3)	.	.	.	yes
C10	C17	C18	119.9 (3)	.	.	.	no
C10	C17	C24	116.8 (4)	.	.	.	no
C18	C17	C24	123.1 (4)	.	.	.	no
C17	C18	C19	118.2 (4)	.	.	.	no
C17	C18	C23	124.7 (4)	.	.	.	no
C19	C18	C23	117.0 (4)	.	.	.	no
C18	C19	C20	121.9 (4)	.	.	.	no
C19	C20	C21	120.1 (4)	.	.	.	no
C20	C21	C22	118.8 (4)	.	.	.	no
C21	C22	C23	121.0 (4)	.	.	.	no
C18	C23	C22	121.1 (4)	.	.	.	no
V	C24	C17	73.3 (3)	.	.	.	yes
V	C24	C25	143.9 (3)	.	.	.	yes

V	C24	C31	54.1 (2)	.	.	.	yes	
C17	C24	C25	123.6 (4)	.	.	.	no	
C17	C24	C31	118.0 (4)	.	.	.	no	
C25	C24	C31	118.3 (3)	.	.	.	no	
C24	C25	C26	121.0 (4)	.	.	.	no	
C24	C25	C30	121.5 (4)	.	.	.	no	
C26	C25	C30	117.1 (4)	.	.	.	no	
C25	C26	C27	121.6 (4)	.	.	.	no	
C26	C27	C28	120.1 (4)	.	.	.	no	
C27	C28	C29	119.1 (4)	.	.	.	no	
C28	C29	C30	120.7 (5)	.	.	.	no	
C25	C30	C29	121.3 (4)	.	.	.	no	
V	C31	C24	88.0 (3)	.	.	.	yes	
V	C31	C32	149.0 (3)	.	.	.	yes	
C24	C31	C32	123.0 (4)	.	.	.	no	
C31	C32	C33	122.5 (4)	.	.	.	no	
C31	C32	C37	120.5 (4)	.	.	.	no	
C33	C32	C37	117.0 (4)	.	.	.	no	
C32	C33	C34	121.8 (4)	.	.	.	no	
C33	C34	C35	119.3 (4)	.	.	.	no	
C34	C35	C36	119.8 (4)	.	.	.	no	
C35	C36	C37	120.9 (5)	.	.	.	no	
C32	C37	C36	121.1 (4)	.	.	.	no	
V	C1	H1	123.00	.	.	.	no	
C2	C1	H1	126.00	.	.	.	no	
C5	C1	H1	126.00	.	.	.	no	
V	C2	H2	122.00	.	.	.	no	
C1	C2	H2	126.00	.	.	.		no
C3	C2	H2	126.00	.	.	.		no
V	C3	H3	122.00	.	.	.		no
C2	C3	H3	126.00	.	.	.		no
C4	C3	H3	126.00	.	.	.		no
V	C4	H4	121.00	.	.	.		no
C3	C4	H4	126.00	.	.	.		no
C5	C4	H4	126.00	.	.	.		no
C5	C6	H6A	110.00	.	.	.		no
C5	C6	H6B	110.00	.	.	.		no
C7	C6	H6A	110.00	.	.	.		no
C7	C6	H6B	110.00	.	.	.		no
H6A	C6	H6B	108.00	.	.	.		no
N	C7	H7A	109.00	.	.	.		no
N	C7	H7B	109.00	.	.	.		no
C6	C7	H7A	109.00	.	.	.		no
C6	C7	H7B	109.00	.	.	.		no
H7A	C7	H7B	108.00	.	.	.		no
N	C8	H8A	109.00	.	.	.		no
N	C8	H8B	109.00	.	.	.		no
N	C8	H8C	109.00	.	.	.		no
H8A	C8	H8B	109.00	.	.	.		no
H8A	C8	H8C	109.00	.	.	.		no
H8B	C8	H8C	109.00	.	.	.		no
N	C9	H9A	109.00	.	.	.		no
N	C9	H9B	109.00	.	.	.		no
N	C9	H9C	109.00	.	.	.		no
H9A	C9	H9B	109.00	.	.	.		no
H9A	C9	H9C	109.00	.	.	.		no
H9B	C9	H9C	109.00	.	.	.		no
C11	C12	H12	119.00	.	.	.		no
C13	C12	H12	119.00	.	.	.		no
C12	C13	H13	120.00	.	.	.		no
C14	C13	H13	120.00	.	.	.		no

C13	C14	H14	120.00	.	.	.	no
C15	C14	H14	120.00	.	.	.	no
C14	C15	H15	120.00	.	.	.	no
C16	C15	H15	120.00	.	.	.	no
C11	C16	H16	120.00	.	.	.	no
C15	C16	H16	120.00	.	.	.	no
C18	C19	H19	119.00	.	.	.	no
C20	C19	H19	119.00	.	.	.	no
C19	C20	H20	120.00	.	.	.	no
C21	C20	H20	120.00	.	.	.	no
C20	C21	H21	121.00	.	.	.	no
C22	C21	H21	121.00	.	.	.	no
C21	C22	H22	119.00	.	.	.	no
C23	C22	H22	119.00	.	.	.	no
C18	C23	H23	119.00	.	.	.	no
C22	C23	H23	119.00	.	.	.	no
C25	C26	H26	119.00	.	.	.	no
C27	C26	H26	119.00	.	.	.	no
C26	C27	H27	120.00	.	.	.	no
C28	C27	H27	120.00	.	.	.	no
C27	C28	H28	120.00	.	.	.	no
C29	C28	H28	120.00	.	.	.	no
C28	C29	H29	120.00	.	.	.	no
C30	C29	H29	120.00	.	.	.	no
C25	C30	H30	119.00	.	.	.	no
C29	C30	H30	119.00	.	.	.	no
C32	C33	H33	119.00	.	.	.	no
C34	C33	H33	119.00	.	.	.	no
C33	C34	H34	120.00	.	.	.	no
C35	C34	H34	120.00	.	.	.	no
C34	C35	H35	120.00	.	.	.	no
C36	C35	H35	120.00	.	.	.	no
C35	C36	H36	120.00	.	.	.	no
C37	C36	H36	120.00	.	.	.	no
C32	C37	H37	119.00	.	.	.	no
C36	C37	H37	119.00	.	.	.	no

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_diffrn_reflns_theta_full 24.73
_diffrn_measured_fraction_theta_full 1.21
_refine_diff_density_max 1.12(10)
_refine_diff_density_min -0.43

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#===END