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Unprecedented reactivity of an aluminium hydride complex with ArNH₂BH₃

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BRUKER AXS SMART APEX 2 Vers. 1.0-27
R.H. Blessing, Acta Cryst. (1995) A51 33-38
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goodness of fit S are based on F2, conventional R-factors R are based
on F, with F set to zero for negative F2. The threshold expression of
F2 > 2sigma(F2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F2 are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
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C1 C 0.3580(4) 0.1816(3) 0.3883(2) 0.0292(8) Uani 1 1 d . . .
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C2 C 0.4016(4) 0.2963(3) 0.36139(17) 0.0202(6) Uani 1 1 d . . .
C3 C 0.3008(4) 0.3931(3) 0.39469(18) 0.0225(7) Uani 1 1 d . . .
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C5 C 0.1448(4) 0.6033(3) 0.4058(2) 0.0300(8) Uani 1 1 d . . .
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H5B H 0.0440 0.5770 0.4151 0.045 Uiso 1 1 calc R . .
H5C H 0.1229 0.6810 0.3719 0.045 Uiso 1 1 calc R . .
C6 C 0.6132(4) 0.1984(3) 0.27036(18) 0.0197(6) Uani 1 1 d . . .
C7 C 0.5583(4) 0.2012(3) 0.20293(18) 0.0229(7) Uani 1 1 d . . .
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C10 C 0.8138(4) 0.0034(3) 0.2649(2) 0.0276(7) Uani 1 1 d . . .
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C11 C 0.7419(4) 0.1009(3) 0.30160(18) 0.0213(6) Uani 1 1 d . . .
C12 C 0.4218(5) 0.3074(3) 0.1668(2) 0.0287(8) Uani 1 1 d . . .
H12 H 0.4252 0.3802 0.1815 0.034 Uiso 1 1 calc R . .
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H13B H 0.1607 0.3644 0.1685 0.067 Uiso 1 1 calc R . . .
H13C H 0.2193 0.2956 0.2483 0.067 Uiso 1 1 calc R . . .
C14 C 0.4552(6) 0.3259(4) 0.0816(2) 0.0439(10) Uani 1 1 d . . .
H14A H 0.4337 0.2625 0.0650 0.066 Uiso 1 1 calc R . . .
H14B H 0.5738 0.3235 0.0650 0.066 Uiso 1 1 calc R . . .
H14C H 0.3796 0.4037 0.0603 0.066 Uiso 1 1 calc R . . .
C15 C 0.8102(4) 0.0953(3) 0.37247(19) 0.0234(7) Uani 1 1 d . . .
H15 H 0.7360 0.1659 0.3949 0.028 Uiso 1 1 calc R . . .
C16 C 0.9918(4) 0.1033(4) 0.3543(2) 0.0342(8) Uani 1 1 d . . .
H16A H 1.0691 0.0309 0.3370 0.051 Uiso 1 1 calc R . . .
H16B H 1.0278 0.1108 0.3992 0.051 Uiso 1 1 calc R . . .
H16C H 0.9945 0.1732 0.3151 0.051 Uiso 1 1 calc R . . .
C17 C 0.8071(5) -0.0178(3) 0.4305(2) 0.0330(8) Uani 1 1 d . . .
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H17B H 0.8390 -0.0130 0.4771 0.049 Uiso 1 1 calc R . . .
H17C H 0.8878 -0.0879 0.4117 0.049 Uiso 1 1 calc R . . .
C18 C 0.3793(4) 0.6736(3) 0.28580(17) 0.0202(6) Uani 1 1 d . . .
C19 C 0.4254(4) 0.7505(3) 0.31674(19) 0.0228(7) Uani 1 1 d . . .
C20 C 0.3982(5) 0.8685(3) 0.2787(2) 0.0291(8) Uani 1 1 d . . .
H20 H 0.4309 0.9215 0.2982 0.038 Uiso 1 1 calc R . . .
C21 C 0.3253(5) 0.9096(3) 0.2136(2) 0.0328(8) Uani 1 1 d . . .
H21 H 0.3084 0.9900 0.1884 0.043 Uiso 1 1 calc R . . .
C22 C 0.2767(5) 0.8331(3) 0.1850(2) 0.0288(8) Uani 1 1 d . . .
H22 H 0.2237 0.8627 0.1408 0.038 Uiso 1 1 calc R . . .
C23 C 0.3035(4) 0.7143(3) 0.21929(18) 0.0232(7) Uani 1 1 d . . .
C24 C 0.4971(4) 0.7140(3) 0.39035(19) 0.0258(7) Uani 1 1 d . . .
H24 H 0.5094 0.6277 0.4101 0.031 Uiso 1 1 calc R . . .
C25 C 0.6722(5) 0.7305(4) 0.3805(2) 0.0357(9) Uani 1 1 d . . .
H25A H 0.7489 0.6854 0.3432 0.054 Uiso 1 1 calc R . . .
H25B H 0.7185 0.7012 0.4282 0.054 Uiso 1 1 calc R . . .
H25C H 0.6614 0.8154 0.3637 0.054 Uiso 1 1 calc R . . .
C26 C 0.3773(5) 0.7869(4) 0.4482(2) 0.0389(9) Uani 1 1 d . . .
H26A H 0.3699 0.8712 0.4312 0.058 Uiso 1 1 calc R . . .
H26B H 0.4219 0.7571 0.4963 0.058 Uiso 1 1 calc R . . .
H26C H 0.2639 0.7787 0.4539 0.058 Uiso 1 1 calc R . . .
C27 C 0.2430(5) 0.6343(3) 0.1869(2) 0.0288(8) Uani 1 1 d . . .
H27 H 0.3029 0.5497 0.2088 0.035 Uiso 1 1 calc R . . .
C28 C 0.0533(6) 0.6553(5) 0.2094(3) 0.0515(12) Uani 1 1 d . . .
H28A H -0.0093 0.7374 0.1879 0.077 Uiso 1 1 calc R . . .
H28B H 0.0279 0.6428 0.2639 0.077 Uiso 1 1 calc R . . .
H28C H 0.0190 0.5993 0.1908 0.077 Uiso 1 1 calc R . . .
C29 C 0.2871(7) 0.6491(5) 0.1027(3) 0.0532(12) Uani 1 1 d . . .
H29A H 0.2208 0.7288 0.0793 0.080 Uiso 1 1 calc R . . .
H29B H 0.2601 0.5885 0.0854 0.080 Uiso 1 1 calc R . . .
H29C H 0.4087 0.6394 0.0891 0.080 Uiso 1 1 calc R . . .
N1 N 0.5319(3) 0.3018(2) 0.30718(14) 0.0175(5) Uani 1 1 d . . .
N2 N 0.4124(3) 0.5474(2) 0.31995(14) 0.0187(5) Uani 1 1 d . . .
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C32 C 0.6939(8) 0.8747(5) 0.0479(3) 0.0625(14) Uani 1 1 d . . .
H32 H 0.5946 0.9097 0.0793 0.094 Uiso 1 1 calc R . . .
C33 C 0.7794(8) 0.9450(5) -0.0002(3) 0.0755(19) Uani 1 1 d . . .
H33 H 0.7396 1.0287 -0.0015 0.113 Uiso 1 1 calc R . . .
C31 C 0.7494(10) 0.7557(6) 0.0512(4) 0.080(2) Uani 1 1 d . . .
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C34 C 0.9209(8) 0.8979(6) -0.0464(3) 0.0730(19) Uani 1 1 d . . .
H34 H 0.9802 0.9479 -0.0794 0.110 Uiso 1 1 calc R . . .
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H201 H 0.743(5) 0.504(3) 0.314(2) 0.027(10) Uiso 1 1 d . . .
H101 H 0.625(6) 0.517(4) 0.198(2) 0.042(12) Uiso 1 1 d . . .
H102 H 0.787(6) 0.370(4) 0.226(3) 0.044(12) Uiso 1 1 d . . .
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H202 H 0.736(6) 0.354(4) 0.368(3) 0.051(13) Uiso 1 1 d . . .

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C27 0.0315(18) 0.0234(18) 0.0310(18) -0.0081(14) -0.0124(15) -0.0011(15)
C28 0.040(2) 0.060(3) 0.068(3) -0.028(3) -0.005(2) -0.023(2)
C29 0.065(3) 0.068(3) 0.037(2) -0.017(2) -0.011(2) -0.026(3)
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N2 0.0178(12) 0.0184(13) 0.0198(13) -0.0044(10) -0.0023(10) -0.0050(10)
A11 0.0147(4) 0.0164(5) 0.0210(5) -0.0039(4) -0.0011(3) -0.0047(4)
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C33 0.093(4) 0.048(3) 0.057(3) -0.005(3) 0.027(3) -0.009(3)
C31 0.092(5) 0.057(4) 0.107(5) 0.015(4) -0.066(4) -0.036(4)
C34 0.070(4) 0.070(4) 0.039(3) 0.008(2) 0.007(2) 0.007(3)
C35 0.064(4) 0.103(6) 0.089(5) -0.059(4) -0.046(4) 0.037(4)
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are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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C29 H29B 0.9800 . ?
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