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Escobar, Gerardo; Ortega, Romeo; Schaft, Arjan J. van der

Published in:
Proceedings of the 24th Annual Conference of the IEEE Industrial Electronics Society, 1998

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Document Version
Publisher's PDF, also known as Version of record

Publication date:
1998

Link to publication in University of Groningen/UMCG research database

Citation for published version (APA):

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A Saturated Output Feedback Controller for the Three Phase Voltage Sourced Reversible Boost Type Rectifier

Gerardo Escobar, Romeo Ortega and Arjan J. van der Schaft

Abstract — In this article, we present a saturating controller to regulate the output voltage load in a three phase Boost type rectifier. The controller only needs the output voltage signal to be implemented. Moreover, by forcing the inductance currents to track desired suitable sinusoidal signals in phase with the input source voltages, the controller can ensure a near the unity power factor functioning of the system. The saturation feature in this controller is motivated by the fact that the allowed combinations of switches in the rectifier circuit define a finite set of allowed control vectors, moreover, the convex combinations of these vectors raise up a convex hull in the space of control inputs, an hexagon in this example. Thus, based upon the assumption of fast switching, we can ensure that any control vector lying inside this hexagon, and much more, inside its inscrit circle, can be physically implementable by means of a PWM strategy or a convex combination of the allowed control vectors.

I. Introduction

In many processes the controllers are restricted to live in finite sets. This is the case in most of the circuits in the field of power electronics, where the control input is normally a binary signal to be introduced in the gate of a thyristor acting as a switch. Classical examples of these systems are the DC-DC converters, AC-DC converters better known as rectifiers, DC-AC converters more frequently referred as inverters, among others.

In this paper we present a saturated controlled that preserves stability of the three phase boost type rectifier. The finite number of allowed switch positions in the circuit, yields a finite set of allowed control vectors, which define a convex hull in the space of the control inputs. Thus, assuming the switches can commute fast enough, we can say that the only implementable control vectors are those who are bounded by the boundaries of this convex hull, for instance they can be implemented via a PWM strategy or by means of a convex combination of the allowed control vectors. Better to consider the convex hull boundaries to propose a bound for a saturated control, we consider the inscrit circle to the convex hull, thus yielding an easier condition to analyze since only its radium is considered. Furthermore, by defining a reference signal tracking problem on the input currents of the converter, the power factor can be made very close to unity as long as the tracked signal is in phase with the rectified input voltages. The load voltage DC component is selected accordind to a given condition on the parameters, which in fact, implies that at least in the steady state, the control vector lies inside the inscrit circle.

The required reference signal amplitude for the input currents is determined via a steady state analysis and a partial system inversion.

This work was motivated by the seminal paper [4] where the problem of output voltage regulation in the three phase rectifier is formulated and some guidelines are given to implement a controller based on the definition of subspaces in the control input space. Later in [3] they presented an approach based on the concept of sliding modes and the computation of the equivalent control.

The rest of the paper is organized as follows: In section 2 the formulation of the problem is given. The model of the rectifier is studied in detail, the αβ-transformation is used in order to express the model in a reduced frame, and finally the control objective is presented. Section 3 is devoted to the controller design. In section 4 the main result of the paper is presented. The proposed controller is analyzed and stability proofs are given. In section 5 simulations results are provided for assessing the performance of the proposed saturated control law. Finally, in section 6, we give some conclusions and further research.

II. Problem formulation

A. Mathematical model

Consider the three phase Boost type rectifier shown in Figure 1. This circuit is composed in its main part by a bridge of three legs, where each leg contains two switches connected in cascade. We will refer to this switches as the upper switch and the lower switch. In the special case of the rectifier, the switches in each leg work in a complementary way, that is, when one of them is connected, i.e., in the ON position, the other is disconnected, i.e., in the OFF position. For this reason, we assign to each leg only one control input, namely δ1, δ2 and δ3 taking only two values each one. We
will assign the value -1 in the case the upper switch in the OFF position and the lower switch in the ON position, and +1 in the other case (\(\delta_i = -1, i = 1, 2, 3\)).

The permissible combinations of the switches connections are given in table 1, all they form eight possible choices.

Also assume that the vector of source line voltages is composed by purely sinusoidal signals, i.e.,

\[
\begin{bmatrix}
  v_1 \\
v_2 \\
v_3
\end{bmatrix} = \begin{bmatrix}
  V \cos(wt) \\
v_2 \cos(wt - \frac{2}{3} \pi) \\
v_2 \cos(wt - \frac{2}{3} \pi)
\end{bmatrix}
\]

where \(V\) is the amplitude of the voltage signal in [Volts] and \(w\) its frequency in [rad/sec].

For our purpose we will consider that the output current load is due to a purely resistive element, i.e., \(I_o = V_c / R\), where \(R\) represents the load resistance.

**B. Coordinate Transformation. \(a\beta\)-Model**

Consider the commonly called Blondel-Park transformation or 3/2-transformation given by,

\[
P = \frac{2}{3} \begin{bmatrix}
  1 & -1 & -1 \\
  0 & \sqrt{2} & -\frac{\sqrt{2}}{2} \\
  0 & -\frac{\sqrt{2}}{2} & \frac{\sqrt{2}}{2}
\end{bmatrix}
\]

We apply the above transformation to the model (2.2) in the following way,

\[
x = P \begin{bmatrix}
i_1 \\
i_2
\end{bmatrix}, \quad v = P \begin{bmatrix} v_1 \\
v_2
\end{bmatrix}, \quad u = P \begin{bmatrix}\delta_1 \\
\delta_2 \\
\delta_3
\end{bmatrix}
\]

\[
x = \begin{bmatrix} x_1, x_2 \end{bmatrix}^T, \quad v = \begin{bmatrix} v_1, v_2 \end{bmatrix}^T \quad \text{and} \quad u = \begin{bmatrix} u_1, u_2 \end{bmatrix}.
\]

This transformation together with the variable change \(y = v_c\), yields the following model which is now expressed in a coordinate set referred to a fixed frame,

\[
L_i \frac{d}{dt} x_1 = -r \begin{bmatrix} x_1 \\
x_2 \end{bmatrix} + \begin{bmatrix} v_2 \\
v_1\end{bmatrix} - \frac{y}{2} \begin{bmatrix} u_1 \\
u_2
\end{bmatrix}
\]

\[
C \frac{d}{dt} y = \frac{1}{2} \begin{bmatrix} u_1, u_2 \end{bmatrix} \begin{bmatrix} x_1 \\
x_2 \end{bmatrix} - I_o
\]

Notice that in order to arrive to this model the following fact has been used,

\[
\delta^T i = u^T x
\]

which stems from the fact that transformation (2.5) is power conserving.

For our purpose we will consider that the output current load is due only to a purely resistive element, i.e., \(I_o = V_c / R\), where \(R\) represents the load resistance. This yields the model,

\[
L_i \frac{d}{dt} x_1 = -r \begin{bmatrix} x_1 \\
x_2 \end{bmatrix} + \begin{bmatrix} v_2 \\
v_1\end{bmatrix} - \frac{y}{2} \begin{bmatrix} u_1 \\
u_2
\end{bmatrix}
\]

\[
C \frac{d}{dt} y = \frac{1}{2} \begin{bmatrix} u_1, u_2 \end{bmatrix} \begin{bmatrix} x_1 \\
x_2 \end{bmatrix} - \frac{y}{R}
\]

Line source voltages \([v_1, v_2]^T\) take now the values,

\[
\begin{bmatrix} v_1 \\
v_2
\end{bmatrix} = E \begin{bmatrix} \cos(wt) \\
\sin(wt)
\end{bmatrix}
\]
or in matrix form,
\[
v = e^{jwt} \begin{bmatrix} E \\ 0 \end{bmatrix}, \quad e^{jwt} = \begin{bmatrix} \cos(w t) & -\sin(w t) \\ \sin(w t) & \cos(w t) \end{bmatrix}
\]
where we have defined \(E = \sqrt{\frac{1}{2}} V\) by simplicity.

Table 2 resumes the transformation of the control input vectors. The vectors in the new frame, i.e., \(u = [u_1, u_2]^T\), form the commonly called input space which in this specific problem can be drawn on a plane as shown in figure 2. We will refer to this vectors as the allowed control vectors, they form a convex hull, an hexagon in this special case. Moreover, inscribed to this hexagon, there is an inscribed circle with radius equal to \(\sqrt{2}\).

<table>
<thead>
<tr>
<th>(N_o)</th>
<th>(\delta_1)</th>
<th>(\delta_2)</th>
<th>(\delta_3)</th>
<th>(u_1)</th>
<th>(u_2)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(U_0)</td>
<td>-1</td>
<td>-1</td>
<td>-1</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>(U_1)</td>
<td>1</td>
<td>-1</td>
<td>-1</td>
<td>(\sqrt{\frac{1}{2}})</td>
<td>0</td>
</tr>
<tr>
<td>(U_2)</td>
<td>1</td>
<td>1</td>
<td>-1</td>
<td>(\sqrt{\frac{1}{2}})</td>
<td>(\sqrt{2})</td>
</tr>
<tr>
<td>(U_3)</td>
<td>-1</td>
<td>1</td>
<td>-1</td>
<td>(-\sqrt{\frac{1}{2}})</td>
<td>(\sqrt{2})</td>
</tr>
<tr>
<td>(U_4)</td>
<td>-1</td>
<td>-1</td>
<td>1</td>
<td>(-\sqrt{\frac{1}{2}})</td>
<td>0</td>
</tr>
<tr>
<td>(U_5)</td>
<td>-1</td>
<td>-1</td>
<td>1</td>
<td>(-\sqrt{\frac{1}{2}})</td>
<td>(-\sqrt{2})</td>
</tr>
<tr>
<td>(U_6)</td>
<td>1</td>
<td>1</td>
<td>1</td>
<td>0</td>
<td>(\sqrt{2})</td>
</tr>
</tbody>
</table>

Table 2: Permitted switch positions in the \(\alpha\beta\)-model

C. Control Objective

The control objective is to propose a control vector \(u(t)\) of the system modeled by equations (2.7,2.8), whose goal is twofold. First, to drive the output capacitor voltage to a desired constant value, i.e., \(y(t) \to V_d\) as \(t \to \infty\), where \(V_d\) is a constant desired output voltage. Second, the control input vector \(u(t)\), should be designed in such a way that the inductance currents \(x(t) \to x_d(t)\) as \(t \to \infty\) where \(x_d(t) \in C^1\) is a time varying vector of desired currents with constant amplitude \(I_d\) yet to be defined. This vector is turning counterclockwise at a frequency \(w\) and in phase with the source line voltage \(v = [u_1, u_2]\), in order to ensure a near the unity power factor functioning.

The desired currents vector \(x_d = [x_{1d}, x_{2d}]^T\) is described by,
\[
x_d = e^{jwt} \begin{bmatrix} I_d \\ 0 \end{bmatrix}
\]

or more explicitly,
\[
x_{1d} = I_d \cos(w t), \quad x_{2d} = I_d \sin(w t)
\]
where \(I_d\) is a constant value yet to be determined.

Moreover, due to the fact that the only implementable control vectors are those contained in the hexagon (see Fig. 2), then the amplitude of the computed control vector should be restricted, and for easy of analysis we will consider the radius of the inscribed circle, i.e., \(||u(t)|| \leq \sqrt{2}||\).

III. Controller design

Consider that the desired currents given by (2.9) fulfill the currents equation (2.7), that is,
\[
L\dot{x}_d = -r x_d + v - \frac{y}{2} u^*
\]
where according to eq. (2.9),
\[
\dot{x}_d = wJ e^{jwt} \begin{bmatrix} I_d \\ 0 \end{bmatrix} = wJ x_d
\]

Solving from the last expression for \(u\), we obtain,
\[
u^* = \frac{2}{y} (v - r x_d - wL J x_d)
\]
being \(u^*\) a control signal which needs still to be saturated.

Notice that this expression is divided by \(y\). This will make our result local since we should restrict the output voltage to be \(y > c\), being \(c\) a constant strictly bigger than zero.

Notice that \(u^*\) can be written as a rotating vector in the following way,
\[
u^* = \frac{2}{y} \left( v - r x_d - wL J x_d \right)
\]
and finally,
\[
u^* = \frac{2}{y} e^{jwt} \begin{bmatrix} 1 \\ 0 \end{bmatrix}
\]
where,
\[
a = \sqrt{(E - r I_d)^2 + w^2 L^2 P_d}, \quad \phi = \tan^{-1} \left( \frac{wL I_d}{E - r I_d} \right)
\]
\[
\cos(\phi) = \frac{E - r I_d}{a}, \quad \sin(\phi) = \frac{wL I_d}{a}
\]
In order to ensure that the controller is contained in the inscribed circle, we propose to saturate only the amplitude of the control vector (3.6) and to maintain the angle. Thus, the resulting controller to be applied takes the form,
\[
u = \begin{cases} 2 \frac{a}{y} e^{jwt} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \cos(\phi) \epsilon_1, & ||u^*|| \leq \sqrt{2} \\ \frac{2}{\sqrt{2}} e^{jwt} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \cos(\phi) \epsilon_1, & ||u^*|| > \sqrt{2} \end{cases}
\]
where \(\epsilon_1 = \begin{bmatrix} 1, 0 \end{bmatrix}\) is the unitary canonical vector.

Now we analyze the the steady state response of the system in order to compute \(I_d\), that is, eq. (2.8) is evaluated for
\[ x = \bar{x}, y = \bar{y}, V_d \] and \( u(x, y, t) = u(\bar{x}, \bar{y}, t) = u(x_d, V_d, t) \).

This yields,

\[
0 = \frac{1}{2} \begin{bmatrix} 1 & 0 \end{bmatrix} e^{-j(\omega t - \phi)} e^{j\omega t} \begin{bmatrix} I_d & 0 \end{bmatrix} - \frac{V_d^2}{R} \quad (3.10)
\]

\[
= \frac{I_d(E - r I_d)}{V_d} - \frac{V_d^2}{R} \quad (3.11)
\]

The last equation has two solutions for \( I_d \), nevertheless, only one of them is physically meaningful, and is given by,

\[
I_d = \frac{E}{2r} - \sqrt{\frac{E^2}{4r^2} - \frac{V_d^2}{R}} \quad (3.12)
\]

With the results above we can state our main result.

IV. Main result

Proposition IV.1 Consider the system described by eqs. (2.7,2.8) in closed loop with the saturated controller (3.9). Then the output voltage \( y \) locally asymptotically reaches the desired constant value \( V_d \) which is chosen such that the following condition is satisfied,

\[
V_d^2 > 2 \left( 1 + \frac{r^2 + 0.5r^2}{2w^2 L_2^2} \right) (E^2 + w^2 L_2^2 I_d^2) \quad (4.1)
\]

where \( I_d \) is computed according to (3.12).

Moreover, the inductance currents vector \( x = [x_1, x_2]^T \) locally asymptotically tracks the rotating desired currents vector \( x_d = [x_{d1}, x_{d2}] \) given by (2.9), thus ensuring a near the unity power factor functioning.

A. Proof:

The proof is divided into two parts, first we consider the case when the control vector \( ||u^*|| \leq \sqrt{2} \), and thus we chose \( u = u^* \). Second, we analyze the case \( ||u^*|| > \sqrt{2} \), so \( u \) is chosen as the vector in the same direction as \( u^* \) but with amplitude \( \sqrt{2} \).

Case 1:

In this case, the controller is given by (3.3),

\[
u = u^* - \frac{r}{L} (v - rx_d - wLx_d)
\]

This control in closed loop with the system (2.7,2.8), yields the following error dynamics,

\[
\dot{\bar{x}} = -\frac{r}{L} \bar{x} \quad (4.2)
\]

\[
C_g \dot{y} = \frac{1}{y} (v^2 - rx_d^2 + wLx_d^2 J)x - \frac{y}{R} \quad (4.3)
\]

where \( \bar{x} = \bar{x} - x_d \). Let's define \( \bar{z} = \frac{1}{y} y^2 \), then \( \dot{\bar{z}} = \dot{y}y \), thus the second eq. in the error dynamics become,

\[
C \dot{\bar{z}} = v^T \bar{x} + v^T x_d - rx_d^2 \bar{z} - r I_d \bar{z} + wLx_d^2 J \bar{z} - \frac{2\bar{z}}{R} \quad (4.4)
\]

where we used the fact that \( v^T x_d = EI_d \).

Analyzing the equilibrium point in the error dynamics,

\[
0 = \bar{z} \quad (4.5)
\]

\[
0 = EI_d - r I_d - \frac{2\bar{z}}{R} \quad (4.6)
\]

From the first equation, \( \bar{z} = 0 \), and from the second equation with \( \bar{z} = \frac{V_d^2}{R} \),

\[
0 = EI_d - r I_d^2 - \frac{V_d^2}{R} \quad (4.7)
\]

which coincides with (3.11).

Thus, by defining \( \bar{z} = \bar{z} - \bar{z} \), the error dynamics can be written finally as,

\[
\dot{\bar{z}} = -\frac{r}{L} \bar{z} \quad (4.8)
\]

\[
C \dot{\bar{z}} = v^T \bar{x} + v^T x_d - rx_d^2 \bar{z} + wLx_d^2 J \bar{z} - \frac{2\bar{z}}{R} \quad (4.9)
\]

whose equilibrium point is the origin.

Consider now the following change of coordinates,

\[
\psi_1 = x_{d1} \bar{z} \quad (4.10)
\]

\[
\psi_2 = x_{d2} \bar{z} \quad (4.11)
\]

The error dynamics is then transformed to,

\[
\dot{\psi}_1 = -\frac{r}{L} \psi_1 - w \psi_2 \quad (4.12)
\]

\[
\dot{\psi}_2 = -\frac{r}{L} \psi_2 + w \psi_1 \quad (4.13)
\]

\[
\dot{\bar{z}} = \frac{E}{C I_d} \psi_1 - \frac{r}{C} \psi_1 + \frac{wL}{C} \psi_2 - \frac{2\bar{z}}{R} \quad (4.14)
\]

which can be written in matrix form as follows,

\[
\begin{bmatrix}
\dot{\psi}_1 \\
\dot{\psi}_2 \\
\dot{\bar{z}}
\end{bmatrix} =
\begin{bmatrix}
-\frac{r}{L} & -w & 0 \\
w & -\frac{r}{L} & 0 \\
\frac{E}{C I_d} & \frac{wL}{C} - \frac{2}{R} & -\frac{2}{R}
\end{bmatrix}
\begin{bmatrix}
\psi_1 \\
\psi_2 \\
\bar{z}
\end{bmatrix}
\]

Case 2:

In this case \( ||u^*|| > \sqrt{2} \), then the controller is selected according to (3.9) to be,

\[
u = \sqrt{2} e^{-j(\omega t - \phi)} \begin{bmatrix} 1 \\
0
\end{bmatrix}, \quad \phi = \text{atan} \left( \frac{wL I_d}{E - r I_d} \right) \quad (4.16)
\]

For this part of the proof we will require the following lemma.

Fig. 3: Block diagram of system considered in the lemma
Lemma IV.2 Consider the system (see Fig. 3) described by the following dynamics,

\[ \zeta = H(p)\Phi \xi \]  
\[ \eta = \Phi^T \zeta \]

where \( \xi, \eta \in \mathbb{R}; \zeta, \Phi \in \mathbb{R}^2; H(p) \in \mathbb{R}^{2 \times 2}(p) \).

Assume,

\[ \Phi = \begin{bmatrix} \gamma \sin(wt - \theta) \\ \gamma \cos(wt - \theta) \end{bmatrix} \]

Then the system can be expressed as the linear system,

\[ \eta = \Sigma(p)\xi \]

where the new transfer function \( \Sigma(s) \) is defined as,

\[ \Sigma(s) = \frac{s^2}{2} \left[ H(s - jw) + H(s + jw) \right] \]

The system (2.7, 2.5) can be represented by the block diagram of Fig. 4 after some simple manipulations.

![Modified block diagram of the system](image)

Fig. 4: Modified block diagram of the system

In the block diagram in Fig. 4 we can identify an structure similar to that of the lemma IV.2, that is, a linear block being pre and post multiplied by a rotating vector. Thus, by applying the result in this lemma, the whole system can be now expressed as an interconnection of two linear systems as shown in Fig. 5, having by input a signal \( \alpha \) yet to be determined.

![Reduction of the original block diagram to a feedback linear system](image)

Fig. 5: Reduction of the original block diagram to a feedback linear system

In this case,

\[ \Phi = \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} \end{bmatrix} \]

\[ H(s) = \text{diag} \left\{ \frac{1}{Ls + r}, \frac{1}{Ls + r} \right\} \]

Applying the result in lemma IV.2 we obtain,

\[ \Sigma(s) = \frac{1}{2} \left( \frac{Ls + r}{L^2 s^2 + 2Lrs + w^2 L^2 + r^2} \right) \]

The closed loop transfer function of the linear system shown in Fig. 5 is given by,

\[ G(s) = \frac{L^2 s^2 + 2Lrs + w^2 L^2 + r^2}{(Cs + \frac{1}{2}) \left( L^2 s^2 + 2Lrs + \frac{1}{2} s + w^2 L^2 + r^2 + \frac{1}{2} \right)} \]

which is a stable system.

In order to compute the steady state value of the output of this linear system, we should compute before the steady state value of the signal \( \alpha \), which is actually a bounded signal that converges to a constant value as we will see in what follows.

From block diagram in Fig. 4, we see that vector \( v' \) is obtained from the low pass filtering of the rotating vector \( \nu \), i.e.,

\[ v' = \frac{1}{1 + p} e^{j\omega t} \begin{bmatrix} E \\ 0 \end{bmatrix} \]

This gives the following vector, which has been obtained by using the phasor concepts.

\[ v'_s = \frac{E}{b^1} e^{j(\omega t - \beta_1)} \]

where

\[ b_1 = \sqrt{r^2 + w^2 L^2}, \quad \beta_1 = \tan^{-1}(\frac{wL}{r}) \]

\[ \cos(\beta_1) = \frac{r}{b_1}, \quad \sin(\beta_1) = \frac{wL}{b_1} \]

Thus, \( \alpha \) in the steady state is, given by,

\[ \alpha_{ss} = \frac{v'_s}{b_1} \]

\[ \alpha_{ss} = \frac{E}{2ab_1^2} \left[ (E - rId)r + w^2 L^2 I_d \right] \]

We can now compute the steady state value for the system output \( y \) as follows,

\[ y_{ss} = \lim_{s \to 0} sG(s) \frac{\alpha_{ss}}{s} \]

\[ y_{ss} = \frac{RE}{\sqrt{2a(b_1^2 + \frac{r}{2})} \left[ (E - rId)r + w^2 L^2 I_d \right]} \frac{E}{E} \]

As shown in eq. (3.6)

\[ u^* = \frac{2}{y} e^{j(wt - \phi)} \begin{bmatrix} \alpha \\ 0 \end{bmatrix} \]
A condition for this control vector to enter into the circle of radium \( \sqrt{2} \) is that in the steady state,

\[
\|u^*\| < \sqrt{2} \tag{4.36}
\]

That is,

\[
y_{ss} > \sqrt{3}a \tag{4.37}
\]

An upper bound for \( a \) from (3.7) is,

\[
a < \sqrt{E^2 + w^2L^2I_d^2} \tag{4.38}
\]

while a lower bound for \( y_{ss} \) from (4.34) is,

\[
y_{ss} > \frac{V_d^2w^2L^2}{\sqrt{2(E^2 + w^2L^2I_d^2)\left(b_d^2 + \frac{1}{2}\right)}} \tag{4.39}
\]

Thus, the condition (4.37) is implied by the following condition,

\[
\frac{V_d^2w^2L^2}{\sqrt{2(E^2 + w^2L^2I_d^2)\left(b_d^2 + \frac{1}{2}\right)}} > \sqrt{2(E^2 + w^2L^2I_d^2)} \tag{4.40}
\]

From where (4.1) is easily obtained.

**Remark:** Condition (4.1) reveals the amplification characteristic of the Boost rectifier.

**V. Simulation results**

The control strategy discussed before was applied to the rectifier system. Moreover, we propose a set of initial conditions that exhibit the saturating feature of the proposed controller.

Using the software package SIMULINK and the numerical values shown below, digital computer simulations were performed for evaluating the performance of the nonlinear output feedback controller strategy. The simulations were carried out using the actual nonlinear system model (2.7, 2.8) with initial conditions for the currents vector \( z(0) = [0, 0] \) and for the output capacitor voltage \( y(0) = 150\text{Volts} \). This initial conditions put in evidence the saturating feature of the controller proposed.

\[
L = 10\mu\text{H}, \quad \omega_0 = 2\pi 60\text{rad/sec}, \quad C = 1\text{mF}, \quad r = 0.25\Omega
\]

\[
V = 110\text{V}, \quad R = 25\Omega, \quad V_d = 325\text{V}
\]

The first diagram in Fig. 6 shows the phase plot of the inductance currents \( z_2(x_1) \), we can observe that the currents vector reaches the desired currents vector asymptotically. Second diagram in the same figure shows the phase plot of the controls \( u_2(x_1) \), notice that in the transient period the control vector trajectory \( u^* \) in dotted line, can take values that go outside the inscrit circle, thus enabling the saturating feature of the controller proposed. Finally, in the third diagram, the time response of the output capacitor voltage \( y \) is presented. This signal reaches the desired final value \( V_d = 325 \text{Volts} \) in the steady state. Moreover, the non-minimum phase behaviour of the system response can be observed as well.

![Fig. 6: Response of the system under the proposed controller](image-url)