University of Groningen

Taming Mismatches in Inter-agent Distances for the Formation-Motion Control of Second-Order Agents

de Marina, Hector Garcia; Jayawardhana, Bayu; Cao, Ming

Published in:
IEEE Transactions on Automatic Control

DOI:
[10.1109/TAC.2017.2715226](https://doi.org/10.1109/TAC.2017.2715226)

IMPORTANT NOTE: You are advised to consult the publisher's version (publisher's PDF) if you wish to cite from it. Please check the document version below.

Document Version
Publisher's PDF, also known as Version of record

Publication date:
2018

[Link to publication in University of Groningen/UMCG research database](#)

Citation for published version (APA):

de Marina, H. G., Jayawardhana, B., & Cao, M. (2018). Taming Mismatches in Inter-agent Distances for the Formation-Motion Control of Second-Order Agents. *IEEE Transactions on Automatic Control*, 63(2), 449-462. <https://doi.org/10.1109/TAC.2017.2715226>

Copyright

Other than for strictly personal use, it is not permitted to download or to forward/distribute the text or part of it without the consent of the author(s) and/or copyright holder(s), unless the work is under an open content license (like Creative Commons).

The publication may also be distributed here under the terms of Article 25fa of the Dutch Copyright Act, indicated by the "Taverne" license. More information can be found on the University of Groningen website: <https://www.rug.nl/library/open-access/self-archiving-pure/taverne-amendment>.

Take-down policy

If you believe that this document breaches copyright please contact us providing details, and we will remove access to the work immediately and investigate your claim.

Downloaded from the University of Groningen/UMCG research database (Pure): <http://www.rug.nl/research/portal>. For technical reasons the number of authors shown on this cover page is limited to 10 maximum.

Taming Mismatches in Inter-agent Distances for the Formation-Motion Control of Second-Order Agents

Hector Garcia de Marina¹, Member, IEEE, Bayu Jayawardhana², Senior Member, IEEE, and Ming Cao³, Senior Member, IEEE

Abstract—This paper presents the analysis on the influence of distance mismatches on the standard gradient-based rigid formation control for second-order agents. It is shown that, similar to the first-order case as recently discussed in the literature, these mismatches introduce two undesired group behaviors: A distorted final shape and a steady-state motion of the group formation. We show that such undesired behaviors can be eliminated by combining the standard formation control law with distributed estimators. Finally, we show how the mismatches can be effectively employed as design parameters in order to control a combined translational and rotational motion of the formation.

Index Terms—Formation control, motion control, rigid formation, second-order dynamics.

I. INTRODUCTION

RECENT years have witnessed a growing interest in coordinated robot tasks, such as area exploration and surveillance [1], [2], robot formation movement for energy efficiency [3], and tracking and enclosing a target [4], [5]. In many of these team-work scenarios, one of the key tasks for the agents is to form and maintain a prescribed formation shape. Gradient-based control has been widely used for this purpose [6]. In particular, *distance-based* control [7]–[11] has gained popularity since the agents can work with their own local coordinates and the desired shape of the formation under control is *exponentially stable* [12], [13]. However, exponential stability cannot prevent undesired steady-state collective motions, e.g., constant drift, if disturbances, such as biases in the range sensors or equivalently mismatches between the prescribed distances for neighboring

agents, are present. This misbehavior has been carefully studied for agents governed by single integrator dynamics in [14] and [15] and an effective solution to get rid of such misbehavior using estimators has been reported in [16]. The proposed estimator-based tool works without requiring any communication among agents. This is a desired feature since the above mentioned issue with the mismatches cannot usually be solved in a straightforward way by sending back and forth more communication information between the agents for several reasons: The sensing bias can be time-varying due to factors such as the environment's temperature; the same range sensor can produce different readings for the same physical distance in face of random measurement noises, making communication-based correction costly; a continuous (or regular) communication among agents may not even be possible or desired; and the agents may have different clocks complicating the data comparison in real-time computation.

In this paper for second-order agents, i.e., agents modeled by double integrator dynamics, we extend the recent findings in [14]–[17] on *mismatched* formation control, the cancellation of the undesired effects via distributed estimation, and the formation motion control by turning the mismatches into distributed parameters. There are practical benefits justifying such extension. For example, a formation controller employing undirected sensing topologies has inherent stability properties that are not present if *directed* topologies¹ are employed, especially for agents with higher order dynamics [6]. Another key aspect of employing second-order dynamics is that the control actions can be used as the *desired acceleration* in a guidance system feeding the tracking controller of a mechanical system, such as the ones proposed for quadrotors in [18] and [19] or marine vessels in [20]. This clearly simplifies such tracking controllers compared to the case of only providing *desired velocities* derived from first-order agent dynamics.

The extensions presented in this paper require new technical constructions that go much beyond what is needed for first-order agents. For example, a key step in the logic presented in [14]–[17] is based on the fact that the dynamics of the error signal, which measures the distortion with respect to the desired shape, is an autonomous system for first-order agents.

¹For directed topologies, only one agent per edge controls the inter-agent distance. Hence, it is free of mismatches.

Manuscript received November 14, 2016; revised March 14, 2017; accepted June 1, 2017. Date of publication June 15, 2017; date of current version January 26, 2018. This work was supported by the EU INTERREG Program under the auspices of the SMARTBOT Project. The work of M. Cao was also supported by the European Research Council under Grant ERC-StG-307207. Recommended by Associate Editor Z. Sun. (Corresponding author: Hector Garcia de Marina.)

H. G. de Marina is with the Ecole Nationale de l'Aviation Civile, University of Toulouse, Toulouse 31000, France (e-mail: hgdmarina@ieee.org).

B. Jayawardhana and M. Cao are with the Engineering and Technology Institute of Groningen, University of Groningen, Groningen 9747 AG, The Netherlands (e-mail: b.jayawardhana@rug.nl; m.cao@rug.nl).

Color versions of one or more of the figures in this paper are available online at <http://ieeexplore.ieee.org>.

Digital Object Identifier 10.1109/TAC.2017.2715226

This does not hold anymore in the second-order case. Consequently, additional technical steps are developed for extending the results of a *mismatched* formation control to second-order agents.

The problem of motion and formation control can be solved simultaneously if the mismatches are well understood and not treated as disturbances but as design parameters. Indeed, this is the strategy followed in [17], where we have turned mismatches in the prescribed distances into design parameters in order to manipulate the way how the collective motion is realized. The act of turning mismatches to distributed motion parameters allows one to address more complicated problems such as moving a rigid formation (including rotational motion) without leaders, or tracking and enclosing a free target. The desired motion is designed with respect to a frame of coordinates fixed at the desired *rigid-body* shape. This design allows to preserve the ordering of the agents during the motion, e.g., which agent is leading at the front of the group. An important aspect of this approach is that for *low* motion speeds the agents do not need to measure any relative velocities as what is commonly required in swarms of second-order agents [21]. Consequently, the sensing requirements are reduced. It will be shown that the motion parameters for second-order agents can be directly computed from the first-order case as in [17]. Unfortunately, the Lyapunov function for proving the stability of the desired steady-state motion is not as straightforward as in [17], since the *standard* quadratic function, involving the norms of the errors regarding the distortion of the desired shape and the velocity of the agents, can only be used to prove asymptotic [6] but not exponential stability, which is the key property for determining the necessary gains and region of attraction for the formation and motion controller in [17]. Nevertheless, we will be able to show that the stability of the closed-loop formation motion system is indeed exponential for second-order agents too.

The rest of the paper is organized as follows. After some definitions and clarification of notation in Section II, we show in Section III the analysis about the undesired effects on a formation of second-order agents in the presence of small mismatches. It turns out that in addition to a distortion with respect to the desired shape, we have an undesired steady-state collective motion that is consistent with the one described in [22] for first-order agents. In Section IV, we propose two designs for a distributed estimator in order to prevent the mentioned robustness issues. The first design eliminates the undesired steady-state motion and is able to bound the steady-state distortion with respect to a generic rigid desired shape. In particular, this first design completely removes the distortion for the special cases of triangles and tetrahedrons. The second design is less straightforward and requires the calculations of some lower bounds for certain gains. However, it eliminates the undesired steady-state motion and distortion for any desired shape. In Section V, we turn the mismatches into distributed motion parameters in a similar way as in [17] in order to design the stationary motion of the formation without distorting the desired shape. Finally, in order to validate the proposed algorithms from Sections IV and V, simulation results with second-order agents are provided in Section VI.

II. PRELIMINARIES

In this section, we introduce some notations and concepts related to graphs and rigid formations. For a given matrix $A \in \mathbb{R}^{n \times p}$, define $\bar{A} \triangleq A \otimes I_m \in \mathbb{R}^{nm \times pm}$, where the symbol $\otimes$ denotes the Kronecker product, $m = 2$ for the two-dimensional (2-D) formation case or $m = 3$ for the 3-D one, and I_m is the m -dimensional identity matrix. For a stacked vector $x \triangleq [x_1^T \ x_2^T \ \dots \ x_k^T]^T$ with $x_i \in \mathbb{R}^n$, $i \in \{1, \dots, k\}$, we define the diagonal matrix $D_x \triangleq \text{diag}\{x_i\}_{i \in \{1, \dots, k\}} \in \mathbb{R}^{kn \times kn}$. We denote by $|\mathcal{X}|$ the cardinality of the set $\mathcal{X}$ and by $\|x\|$ the Euclidean norm of a vector x . We use $\mathbf{1}_{n \times m}$ and $\mathbf{0}_{n \times m}$ to denote the all-one and all-zero matrix in $\mathbb{R}^{n \times m}$, respectively, and we will omit the subscript if the dimensions are clear from the context.

A. Graphs and Minimally Rigid Formations

We consider a formation of $n \geq 2$ autonomous agents whose positions are denoted by $p_i \in \mathbb{R}^m$. The agents can measure their relative positions with respect to its neighbors. This sensing topology is given by an undirected graph $\mathbb{G} = (\mathcal{V}, \mathcal{E})$ with the vertex set $\mathcal{V} = \{1, \dots, n\}$ and the ordered edge set $\mathcal{E} \subseteq \mathcal{V} \times \mathcal{V}$. The set $\mathcal{N}_i$ of the neighbors of agent i is defined by $\mathcal{N}_i \triangleq \{j \in \mathcal{V} : (i, j) \in \mathcal{E}\}$. We define the elements of the incidence matrix $B \in \mathbb{R}^{|\mathcal{V}| \times |\mathcal{E}|}$ for $\mathbb{G}$ by

$$b_{ik} \triangleq \begin{cases} +1, & \text{if } i = \mathcal{E}_k^{\text{tail}} \\ -1, & \text{if } i = \mathcal{E}_k^{\text{head}} \\ 0, & \text{otherwise} \end{cases}$$

where $\mathcal{E}_k^{\text{tail}}$ and $\mathcal{E}_k^{\text{head}}$ denote the tail and head nodes, respectively, of the edge $\mathcal{E}_k$, i.e., $\mathcal{E}_k = (\mathcal{E}_k^{\text{tail}}, \mathcal{E}_k^{\text{head}})$. A *framework* is defined by the pair $(\mathbb{G}, p)$, where $p = \text{col}\{p_1, \dots, p_n\}$ is the stacked vector of the agents' positions p_i , $i \in \{1, \dots, n\}$. With this last definition at hand, we define the stacked vector of the measured relative positions by

$$z = \bar{B}^T p$$

where each vector $z_k = p_i - p_j$ in z corresponds to the relative position associated with the edge $\mathcal{E}_k = (i, j)$.

For a given stacked vector of desired relative positions $z^* = [z_1^{*T} \ z_2^{*T} \ \dots \ z_{|\mathcal{E}|}^{*T}]^T$, the resulting set $\mathcal{Z}$ of the possible formations with the same shape is defined by

$$\mathcal{Z} \triangleq \{(I_{|\mathcal{E}|} \otimes \mathcal{R}) z^*\} \quad (1)$$

where $\mathcal{R}$ is the set of all rotational matrices in 2-D or 3-D. Roughly speaking, $\mathcal{Z}$ consists of all those formation positions that are obtained by rotating z^* .

Let us now briefly recall the notions of infinitesimally rigid framework and minimally rigid framework from [23]. Define the edge function $f_{\mathbb{G}}$ by $f_{\mathbb{G}}(p) = \text{col}_k(\|z_k\|^2)$ and we denote its Jacobian by

$$2R(z) = 2D_z^T \bar{B}^T \quad (2)$$

where $R(z)$ is called the *rigidity matrix*. A framework $(\mathbb{G}, p)$ is *infinitesimally rigid* if $\text{rank}\{R(z)\} = 2n - 3$ when it is embedded in $\mathbb{R}^2$ or if $\text{rank}\{R(z)\} = 3n - 6$ when it is

Fig. 1. (a) Square without an inner diagonal is not rigid since we can smoothly move the top two nodes while keeping the other two fixed without breaking the distance constraints; (b) Square can be done locally minimally rigid in $\mathbb{R}^2$ if we add an inner diagonal; (c) Tetrahedron in $\mathbb{R}^3$ is infinitesimally and minimally rigid.

embedded in $\mathbb{R}^3$. Additionally, if $|\mathcal{E}| = 2n - 3$ in the 2-D case or $|\mathcal{E}| = 3n - 6$ in the 3-D case, then the framework is called *minimally rigid*. Roughly speaking, the only motions that one can perform over the agents in an infinitesimally and minimally rigid framework, while they are already in the desired shape, are the ones defining translations and rotations of the whole shape. Some graphical examples of infinitesimally and minimally rigid frameworks are shown in Fig. 1. If $(\mathbb{G}, p)$ is infinitesimally and minimally rigid, then, similar to the above, we can define the set of resulting formations $\mathcal{D}$ by

$$\mathcal{D} \triangleq \left\{ z \mid \|z_k\| = d_k, k \in \{1, \dots, |\mathcal{E}|\} \right\}$$

where $d_k = \|z_k^*\|$, $k \in \{1, \dots, |\mathcal{E}|\}$.

Note that in general it holds that $\mathcal{Z} \subseteq \mathcal{D}$. For a desired shape, one can always design $\mathbb{G}$ to make the formation infinitesimally and minimally rigid. In fact, an infinitesimally and minimally rigid framework with two or more vertices in $\mathbb{R}^2$ can always be constructed through the Henneberg construction [24]. In $\mathbb{R}^3$ one can construct a set of infinitesimally and minimally rigid frameworks via insertion starting from a tetrahedron, if each newly added vertex with three newly links forms another tetrahedron as well.

B. Frames of Coordinates

It will be useful for describing the motions of the infinitesimally and minimally rigid formation to define a frame of coordinates fixed to the desired formation itself. We denote by O_g the *global frame* of coordinates fixed at some point of $\mathbb{R}^m$ with some arbitrary fixed orientation. In a similar way, we denote by O_b the *body frame* fixed at the centroid p_c of the desired rigid formation. Furthermore, if we rotate the rigid formation with respect to O_g , then O_b is also rotated in the same manner. Let ${}^b p_j$ denote the position of agent j with respect to O_b . To simplify the notation whenever we represent an agents' variable with respect to O_g , the superscript is omitted, i.e., $p_j \triangleq {}^g p_j$.

III. ROBUSTNESS ISSUES DUE TO MISMATCHES IN FORMATION GRADIENT-BASED CONTROL

A. Gradient Control

Consider a formation of n agents with the sensing topology $\mathbb{G}$ for measuring the relative positions among the agents. The

agents are modeled by a second-order system given by

$$\begin{cases} \dot{p} = v \\ \dot{v} = u \end{cases} \quad (3)$$

where u and v are the stacked vector of control inputs $u_i \in \mathbb{R}^m$ and vector of agents' velocity $v_i \in \mathbb{R}^m$ for $i = \{1, \dots, n\}$ respectively.

In order to control the shape, for each edge $\mathcal{E}_k = (i, j)$ in the infinitesimally and minimally rigid framework, we assign the following potential function V_k

$$V_k(\|z_k\|) = \frac{1}{4}(\|z_k\|^2 - d_k^2)^2$$

with the gradient along p_i or p_j given by

$$\nabla_{p_i} V_k = -\nabla_{p_j} V_k = z_k(\|z_k\|^2 - d_k^2).$$

In order to control the agents' velocities, for each agent i in the infinitesimally and minimally rigid framework, we assign the following (kinetic) energy function T_i

$$T_i(v_i) = \frac{1}{2}\|v_i\|^2$$

with the gradient along v_i be given by

$$\nabla_{v_i} T_i = v_i.$$

One can check that for the potential function

$$\phi(p, v) = \sum_{i=1}^{|\mathcal{V}|} T_i + \sum_{k=1}^{|\mathcal{E}|} V_k \quad (4)$$

the closed-loop system (3) with the control input

$$u = -\nabla_v \phi - \nabla_p \phi \quad (5)$$

becomes the following dissipative Hamiltonian system [25]

$$\begin{cases} \dot{p} = \nabla_v \phi \\ \dot{v} = -\nabla_v \phi - \nabla_p \phi. \end{cases} \quad (6)$$

Considering (4) as the storage energy function of the Hamiltonian system (6), one can show the local asymptotic convergence of the formation to the shape given by $\mathcal{D}$ and all the agents' velocities to zero [6], [26].

Consider the following one-parameter family of dynamical systems $\mathcal{H}_\lambda$ given by

$$\begin{bmatrix} \dot{p} \\ \dot{v} \end{bmatrix} = - \begin{bmatrix} \lambda I_{m|\mathcal{V}|} & -(1-\lambda)I_{m|\mathcal{V}|} \\ (1-\lambda)I_{m|\mathcal{V}|} & I_{m|\mathcal{V}|} \end{bmatrix} \begin{bmatrix} \nabla_p \phi \\ \nabla_v \phi \end{bmatrix} \quad (7)$$

where $\lambda \in [0, 1]$, which defines all convex combinations of the Hamiltonian system (6) and a gradient system. The family $\mathcal{H}_\lambda$ has two important properties summarized in the following lemma.

Lemma 3.1 (see [26]):

- 1) For all $\lambda \in [0, 1]$, the equilibrium set of $\mathcal{H}_\lambda$ is given by the set of the critical points of the potential function ϕ , i.e. $E_{p,v} = \{[p^T \ v^T]^T : \nabla \phi = \mathbf{0}\}$.
- 2) For any equilibrium $[p^T \ v^T]^T \in E_{p,v}$ and for all $\lambda \in [0, 1]$, the numbers of the stable, neutral, and unstable eigenvalues of the Jacobian of $\mathcal{H}_\lambda$ are the same and independent of λ .

This result has been exploited in [13] in order to show the local exponential convergence of $z(t)$ and $v(t)$ to $\mathcal{D}$ and $\mathbf{0}$, respectively. In the following brief exposition, we revisit such exponential stability via a combination of Lyapunov argument and Lemma 3.1, which will play an important role in Section III-B.

Define the distance error corresponding to the edge $\mathcal{E}_k$ by

$$e_k = \|z_k\|^2 - d_k^2 \quad (8)$$

whose time derivative is given by $\dot{e}_k = 2z_k^T \dot{z}_k$. Consider the following autonomous system derived from (7) with $\lambda = 0.5$

$$\begin{aligned} \dot{p} &= -\frac{1}{2}\bar{B}D_z e + \frac{1}{2}v \\ \dot{z} &= -\frac{1}{2}\bar{B}^T \bar{B}D_z e + \frac{1}{2}\bar{B}^T v \end{aligned} \quad (9)$$

$$\dot{e} = -D_z^T \bar{B}^T \bar{B}D_z e + D_z^T \bar{B}^T v \quad (10)$$

$$\dot{v} = -\frac{1}{2}\bar{B}D_z e - v \quad (11)$$

where e is the stacked vector of e_k 's for all $k \in \{1, \dots, |\mathcal{E}|\}$. Define the speed of the agent i by

$$s_i \triangleq \|v_i\|$$

whose time derivative is given by $\dot{s}_i = \frac{v_i^T \dot{v}_i}{s_i}$. The compact form involving all the agents' speed can be written as

$$\dot{s} = D_{\tilde{s}} D_v^T \dot{v} = -\frac{1}{2}D_{\tilde{s}} D_v^T \bar{B}D_z e - D_{\tilde{s}} D_v^T v \quad (12)$$

where s and $\tilde{s}$ are the stacked vectors of s_i 's and $\frac{1}{s_i}$'s for all $i \in \{1, \dots, |\mathcal{V}|\}$, respectively. Now we are ready to show the local exponential convergence to the origin of the speed of the agents and the error distances in the edges.

Lemma 3.2: The origins $e = \mathbf{0}$ and $s = \mathbf{0}$ of the error and speed systems derived from (6) are locally exponentially stable if the given desired shape $\mathcal{D}$ is infinitesimally and minimally rigid.

Proof: Consider e_λ and s_λ as the stacked vectors of the error signals e_k and speeds s_k derived from (7) for any $\lambda \in [0, 1]$, which includes the system (6) for $\lambda = 1$. From the definition of e_k , we know that all the e_λ share the same stability properties by invoking Lemma 3.1, so do s_λ as well.

Consider the following candidate Lyapunov function for the autonomous system (9)–(12) derived from (7) with $\lambda = 0.5$

$$V = \frac{1}{2}\|e\|^2 + \|s\|^2$$

whose time derivative satisfies

$$\begin{aligned} \frac{dV}{dt} &= e^T \dot{e} + 2s^T \dot{s} \\ &= -e^T D_z^T \bar{B}^T \bar{B}D_z e + e^T D_z^T \bar{B}^T v - \underbrace{s^T D_{\tilde{s}} D_v^T \bar{B}D_z e}_{v^T} \\ &\quad - \underbrace{2s^T D_{\tilde{s}} D_v^T v}_{\mathbf{1}_{1 \times |\mathcal{V}|}} \\ &= -e^T D_z^T \bar{B}^T \bar{B}D_z e - 2\|s\|^2. \end{aligned} \quad (13)$$

We first note that the elements of the matrix $D_z^T \bar{B}^T \bar{B}D_z$ are of the form $z_i^T z_j$ with $i, j \in \{1, \dots, |\mathcal{E}|\}$. It has been shown in [14] that for minimally rigid shapes these dot products can be expressed as a (local) smooth functions of e , i.e., $z_i^T z_j = g_{ij}(e)$, allowing us to write $D_z^T \bar{B}^T \bar{B}D_z = Q(e)$. For infinitesimally minimally rigid frameworks $R(z)$ is full rank, so we have that $Q(\mathbf{0}) = R(z^*)R^T(z^*)$ is positive definite with $z^* \in \mathcal{D}$. Moreover, since the eigenvalues of a matrix are continuous functions of their entries, we have that $Q(e)$ is positive definite in the compact set $\mathcal{Q} \triangleq \{e : \|e\|^2 \leq \rho\}$ for some $\rho > 0$. Therefore, if the initial conditions for the error signal and the speed satisfy $\|e(0)\|^2 + \|s(0)\|^2 \leq \rho$, since V is not increasing we have that

$$\frac{dV}{dt} \leq -\sigma_{\min}\|e\|^2 - 2\|s\|^2 \quad (14)$$

where $\sigma_{\min} > 0$ is the smallest (and always positive) eigenvalue of $Q(e)$ in the compact set $\mathcal{Q}$. Hence, we arrive at the local exponential convergence of $e(t)$ and $s(t)$ to the origin. ■

Remark 3.3: It is worth noting that the region of attraction determined by ρ in the proof of Lemma 3.2 for $\lambda = 0.5$ might be different from the one for $\lambda = 1$, since Lemma 3.1 only refers to the Jacobian of (7), i.e., the linearization of the system about the equilibrium.

It can be concluded from the exponential convergence to zero of the speeds of the agents $s(t)$ that the formation will eventually stop. This implies that $p(t)$ will converge exponentially to a finite point in $\mathbb{R}^m$ as $z(t)$ converges exponentially to $\mathcal{D}$.

B. Robustness Issues Caused by Mismatches

Consider a distance-based formation control problem with $n = 2$. It is not difficult to conclude that if the two agents do not share the same prescribed distance to maintain, then an eventual steady-state motion will happen regardless of the dynamics of the agents since the agent with a smaller prescribed distance will chase the other one. Therefore, for $n > 2$ it would not be surprising to observe some collective motion in the steady state of the formation if the neighboring agents do not share the same prescribed distance to maintain.

Consider that two neighboring agents disagree on the desired squared distance d_k^2 in between, namely

$$d_k^{2, \text{tail}} = d_k^{2, \text{head}} - \mu_k \quad (15)$$

where d_k^{tail} and d_k^{head} are the different desired distances that the agents i and j , respectively, in $\mathcal{E}_k = (i, j)$ want to maintain for the same edge, so $\mu_k \in \mathbb{R}$ is a constant mismatch. It can be checked that this disagreement leads to *mismatched potential functions*, therefore, agents i and j do not share anymore the same V_k for $\mathcal{E}_k = (i, j)$, namely

$$V_k^i = \frac{1}{4}(\|z_k\|^2 - d_k^2 + \mu_k)^2, \quad V_k^j = \frac{1}{4}(\|z_k\|^2 - d_k^2)^2$$

under which the control laws for agents i and j use the gradients of V_k^i and V_k^j , respectively, for the edge $\mathcal{E}_k = (i, j)$. In the presence of one mismatch in every edge, the control signal (5) can be rewritten as

$$u = -v - \bar{B}D_z e - \bar{S}_1 D_z \mu \quad (16)$$

where S_1 is constructed from the incidence matrix by setting its -1 elements to 0, and $\mu \in \mathbb{R}^{|\mathcal{E}|}$ is the stacked column vector of μ_k 's for all $k \in \{1, \dots, |\mathcal{E}|\}$. Note that (16) can be also written as

$$u = -v - \overline{B}D_z e - \overline{A}_1(\mu)z \quad (17)$$

where the elements of A_1 are

$$a_{ik} \triangleq \begin{cases} \mu_k, & \text{if } i = \mathcal{E}_k^{\text{tail}} \\ 0, & \text{otherwise.} \end{cases} \quad (18)$$

Inspired by [14], we will show how μ can be seen as a parametric disturbance in an autonomous system whose origin is exponentially stable. Consider the dynamics of the error signal e and the speed of the agents s derived from system (3) with the control input (5)

$$\dot{e} = 2D_z^T \overline{B}^T v \quad (19)$$

$$\dot{s} = -s - D_s D_v^T \overline{B} D_z e \quad (20)$$

and define

$$\alpha_{ki} = z_k^T v_i, \quad k \in \{1, \dots, |\mathcal{E}|\}, i \in \{1, \dots, |\mathcal{V}|\} \quad (21)$$

$$\beta_{ij} = v_i^T v_j, \quad i, j \in \{1, \dots, |\mathcal{V}|\}, i \neq j. \quad (22)$$

We stack all the α_{ki} 's and β_{ij} 's in the column vectors $\alpha \in \mathbb{R}^{|\mathcal{E}||\mathcal{V}|}$ and $\beta \in \mathbb{R}^{\frac{|\mathcal{V}|(|\mathcal{V}|-1)}{2}}$, respectively, and define $\gamma \triangleq [e^T \ s^T \ \alpha^T \ \beta^T]^T$. We recall the result from Lemma 3.2 that for any infinitesimally and minimally rigid framework there exists a neighborhood $\mathcal{U}_z$ about this framework such that for all $z_i, z_j \in \mathcal{U}_z$ with $i, j \in \{1, \dots, |\mathcal{E}|\}$, we can write $z_i^T z_j$ as a smooth function $g_{ij}(e)$. Then using (19)–(22), we get

$$\dot{\gamma} = f(\gamma) \quad (23)$$

which is an autonomous system whose origin is locally exponentially stable using the results from Lemmas 3.1 and 3.2. Obviously, in such a case, the following Jacobian evaluated at $\gamma = \mathbf{0}$

$$J = \left. \frac{\partial f(\gamma)}{\partial \gamma} \right|_{\gamma=0}$$

has all its eigenvalues in the left half complex plane. From the system (3) with control law (16), we can extend (23) but with a parametric disturbance μ because of the third term in (16), namely

$$\dot{\gamma} = f(\gamma, \mu) \quad (24)$$

where $f(\gamma, \mathbf{0})$ is the same as in (23) derived from the gradient controller. Therefore, for a sufficiently small $\|\mu\|$, the Jacobian $\left. \frac{\partial f(\gamma, \mu)}{\partial \gamma} \right|_{\gamma=0}$ is still a stable matrix since the eigenvalues of a matrix are continuous functions of its entries. Although system (24) is still stable under the presence of a small disturbance μ , the equilibrium point is not the origin in general anymore but $\gamma(t) \rightarrow \hat{\gamma}(\mu)$ as t goes to infinity, where $\gamma_\mu \triangleq \hat{\gamma}(\mu)$ is a smooth function of μ with zero value if $\mu = \mathbf{0}$ [27]. This implies that in general each component of e, s, α , and β converges to a nonzero constant with the following two immediate consequences: The formation shape will be distorted, i.e., $e \neq \mathbf{0}$; and the agents

will not remain stationary, i.e., $s \neq \mathbf{0}$. The meaning of having in general nonzero components in α is that the vector velocities of the agents have a fixed relation with the steady-state shape, while the fixed components in β denote a constant relation between the vectors of the agents' velocities. If the disturbance $\|\mu\|$ is sufficiently small, then $\|\gamma_\mu\| < \rho$ for some small $\rho \in \mathbb{R}^+$ implying that $\|e_\mu\| < \rho$, and if further ρ is sufficiently small, then the stationary distorted shape is also infinitesimally and minimally rigid. In addition, since the speeds of the agents converge to a constant (in general nonzero constant), then only translations and/or rotations of the stationary distorted shape can happen.

Theorem 3.4: Consider system (3) with the *mismatched* control input (16) where the desired shape for the formation is infinitesimally and minimally rigid. There exist sufficiently small $\epsilon_1, \epsilon_2 \in \mathbb{R}^+$ such that if the mismatches satisfy $\|\mu\| \leq \epsilon_1$, then the error signal $e(t) \rightarrow e^* \in \mathbb{R}^{|\mathcal{E}|}$ as $t \rightarrow \infty$ with $\|e^*\| \leq \epsilon_2$ such that the steady-state shape of the formation is still infinitesimally and minimally rigid but distorted with respect to the desired one. Moreover, the velocity of the agents $v_i(t) \rightarrow v_i^*(t)$ as $t \rightarrow \infty$, where all the $v_i^*(t), \forall i \in \{1, \dots, n\}$ define a steady-state collective motion that can be captured by constants angular and translational velocities ${}^b\omega^*$ and ${}^b v_c^*$, respectively, where O_b has been placed in the centroid of the resultant distorted infinitesimally and minimally rigid shape.

Proof: We have that system (24), derived from (3) and (16), is self-contained and its origin is locally exponentially stable with $\mu = \mathbf{0}_{|\mathcal{E}| \times 1}$. Then, a small parametric perturbation μ such that $\|\mu\| \leq \epsilon_1$, for some positive small ϵ_1 , does not change the exponential stability property of (24). However, the equilibrium point of (24) at the origin can be shifted. In particular, the new shifted equilibrium is a continuous function of μ , therefore, $e(t) \rightarrow e_\mu \in \mathbb{R}^{|\mathcal{E}|}$ as t goes to infinity, where if ϵ_1 is sufficiently small, then $\|e_\mu\| \leq \epsilon_2$ such that the stationary shape is infinitesimally rigid. We also have that the elements of $s(t) \rightarrow s_\mu$ as t goes to infinity with $s_\mu \in \mathbb{R}^{|\mathcal{V}|}$. Note that the elements of s_μ are nonnegative and in general nonzero. Hence, the agents will not stop moving in the steady state. Since the steady-state shape of the formation locally converges to an infinitesimally and minimally rigid one, from the error dynamics (19) we have that

$$D_{z(t)}^T \overline{B}^T v(t) = R(z(t)) v(t) \rightarrow \mathbf{0}_{m|\mathcal{V}| \times 1}, \quad t \rightarrow \infty$$

therefore, $v(t) \rightarrow v_\mu(t)$ as t goes to infinity, where the non-constant $v_\mu(t) \in \mathbb{R}^{|\mathcal{V}|}$ belongs to the null space of $R(z_\mu(t))$, $z_\mu(t) \in \mathcal{Z}_\mu$ and the set $\mathcal{Z}_\mu$ is defined as in (1) but corresponding to the inter-agent distances of the distorted infinitesimally and minimally rigid shape with $e = e_\mu$. Note that obviously, the evolution of $z(t)$ is a consequence of the evolution of agents' velocities in $v(t)$. The null space of $R(z_\mu)$ corresponds to the infinitesimal motions δp_i for all i such that all the inter-agent distances of the distorted formation are constant, namely

$$R(z_\mu) \delta p = R(z_\mu) v_\mu \delta t = \mathbf{0}_{m|\mathcal{V}| \times 1}$$

or in order words

$$v_i(t) \rightarrow v_{\mu_i}(t), \quad t \rightarrow \infty \quad (25)$$

Fig. 2. Velocities $b\omega^*$ and $b v_c^*$ at the centroid of the tetrahedron rotates and translates the infinitesimally and minimally rigid formation, respectively. If the velocity vectors $b\omega^*$ and $b v_c^*$ are constant, then the formation describes a closed orbit in the plane where the projection of $b v_c^*$ over such a plane and $b\omega^*$ is perpendicular (always the case in 2-D formations) plus a constant drift along the projection of $b v_c^*$ over $b\omega^*$. Note that for the case where $b v_c^*$ and $b\omega^*$ are only parallel or perpendicular, then only the drift or the closed orbit motion, respectively, will occur.

where the velocities $v_{\mu_i}(t)$'s for all the agents are the result of rotating and translating the steady-state distorted shape defined by $\mathcal{Z}_\mu$. This steady-state collective motion of the distorted formation can be represented by the rotational and translational velocities $b\omega^*(t) \in \mathbb{R}^m$ and $b v_c^*(t) \in \mathbb{R}^m$ at the centroid of the distorted rigid shape.

Now we are going to show that the velocities $b\omega^*(t)$ and $b v_c^*(t)$ are indeed constant. By definition we have that $\|v_{\mu_i}(t)\| = s_{\mu_i}$. Since the speed s_{μ_i} for agent i is constant but not its velocity $v_{\mu_i}(t)$, the acceleration $a_{\mu_i}(t) = \frac{dv_{\mu_i}(t)}{dt}$ is perpendicular to $v_{\mu_i}(t)$. The expression of $a_{\mu_i}(t)$ can be derived from (17) and is given by

$$a_{\mu_i}(t) = -v_{\mu_i}(t) - \sum_{k=1}^{|\mathcal{E}|} b_{ik} z_{\mu_k}(t) e_{\mu_k} + \sum_{k=1}^{|\mathcal{E}|} a_{ik} z_{\mu_k}(t) \quad (26)$$

where b_{ik} are the elements of the incidence matrix, and a_{ik} are the elements of the *perturbation* matrix A_1 as defined in (18). From (26), it is clear that the norm $\|a_{\mu_i}(t)\| = \Gamma_i(\gamma_\mu)$ is constant. In addition, since $a_{\mu_i}(t)$ is a continuous function, i.e., the acceleration vector cannot switch its direction, and it is perpendicular to $v_{\mu_i}(t)$, the only possibility for the distorted formation is to follow a motion described by constant velocities $b\omega^*$ and $b v_c^*$ at its centroid. ■

Remark 3.5: In particular, in 2-D the distorted formation will follow a closed orbit if $\Gamma_i(\gamma_\mu) \neq 0$ for all i , or a constant drift if $\Gamma_i(\gamma_\mu) = 0$ for all i . This is due to the fact that in 2-D, $b\omega^*$ and $b v_c^*$ are always perpendicular or equivalently $a_{\mu_i}(t)$ and $v_{\mu_i}(t)$ lie in the same plane. The resultant motion in 3-D is the composition of a drift plus a closed orbit, since $b\omega^*$ and $b v_c^*$ are constant and they do not need to be perpendicular to each other as it can be noted in Fig. 2.

Remark 3.6: Although the disturbance μ acts on the acceleration of the second-order agents, it turns out that the resultant collective motion has the same behavior as for having the disturbance μ acting on the velocity for first-order agents. A detailed description of such a motion related to the disturbance in first-order agents can be found in [17] and [22].

IV. ESTIMATOR-BASED GRADIENT CONTROL

It is obvious that if for the edge $\mathcal{E}_k = (i, j)$ only one of the agents controls the desired inter-agent distance, then a mismatch μ_k cannot be present. However, this solution leads to a directed graph in the sensing topology and the stability of the formation can be compromised [6]. It is desirable to maintain the undirected nature of the sensing topology since it comes with intrinsic stability properties. Then, the control law (16) must be *augmented* in order to remove the undesired effects described in Section III. A solution was proposed in [16] for first-order agents consisting of estimators based on the internal model principle. For each edge $\mathcal{E}_k = (i, j)$, there is only one agent that is assigned to be the *estimating agent*, which is responsible for running an estimator to calculate and compensate the associated μ_k . The estimator proposed in [16] is conservative since the estimator gain has to satisfy a lower-bound (which can be explicitly computed based on the initial conditions) in order to guarantee the exponential stability of the system. Using such distributed estimators, all the undesirable effects are removed at the same time as the estimating agent calibrates its measurements with respect to the nonestimating agent. Another minor issue in the solution of [16] is that the estimating agents cannot be chosen arbitrarily. Here, we are going to present an estimator for second-order agents where the estimating agents and the estimator gain can be chosen arbitrarily (thus, removing the restrictive conditions in [16]). The solution removes the effect of the undesired collective motion but at the cost of not achieving accurately the desired shape $\mathcal{Z}$, where a bound on the norm of the signal error $e(t)$ for all time t , however, can be provided. Furthermore, we will show that for the particular cases of the triangle and tetrahedron, the proposed estimator achieves precisely the desired shapes.

Let us consider the following distributed control law with estimator

$$\begin{cases} \dot{\hat{\mu}} &= \hat{u} \\ u &= -v - \bar{B}D_z e - \bar{S}_1 D_z (\mu - \hat{\mu}) \end{cases}$$

where $\hat{\mu} \in \mathbb{R}^{|\mathcal{E}|}$ is the estimator state and $\hat{u}$ is the estimator input to be designed. Substituting the above control law to (3) gives us the following autonomous system

$$\dot{p} = v \quad (27)$$

$$\dot{v} = -v - \bar{B}D_z e - \bar{S}_1 D_z (\mu - \hat{\mu}) \quad (28)$$

$$\dot{z} = \bar{B}^T \dot{p} = \bar{B}^T v \quad (29)$$

$$\dot{e} = 2D_z^T \dot{z} = 2D_z^T \bar{B}^T v \quad (30)$$

$$\dot{\hat{\mu}} = \hat{u}. \quad (31)$$

Note that the estimating agents are encoded in S_1 , in other words, for the edge $\mathcal{E}_k$ the estimating agent is $\mathcal{E}_k^{\text{tail}}$.

Theorem 4.1: Consider the autonomous system (27)–(31) with nonzero mismatches and a desired infinitesimally and minimally rigid formation shape $\mathcal{Z}$. Consider also the following distributed control action for the estimator $\hat{\mu}$

$$\hat{u} = -D_z^T \bar{S}_1^T v \quad (32)$$

where the estimating agents are chosen arbitrarily. Then, the equilibrium points $(p^*, v^*, z^*, e^*, \hat{\mu}^*)$ of (27)–(31) are asymptotically stable where $v^* = \mathbf{0}$ and the steady-state deformation of the shape satisfies $\|e^*\|^2 \leq 2\|\mu - \hat{\mu}(0)\|^2 + 2\|v(0)\|^2 + \|e(0)\|^2$. Moreover, for the particular cases of triangles and tetrahedrons, the equilibrium $e^* = \mathbf{0}$, i.e., $\hat{\mu}^* = \mu$ and $z^* \in \mathcal{Z}$.

Proof: First we start proving that (32) is a distributed control law. This is clear since the dynamics of $\hat{\mu}_k$ (the k th element of $\hat{\mu}$) are given by

$$\dot{\hat{\mu}}_k = z_k^T v_{\mathcal{E}_k^{\text{tail}}} \quad (33)$$

which implies that the estimating agent $\mathcal{E}_k^{\text{tail}}$ for the edge $\mathcal{E}_k$ is only using the dot product of the associated relative position z_k and its own velocity. Note that using the notation in (21), the above estimator input is given by $\alpha_k \mathcal{E}_k^{\text{tail}}$. Consider the following Lyapunov function candidate

$$V = \frac{1}{2}\|\xi\|^2 + \frac{1}{2}\|v\|^2 + \frac{1}{4}\|e\|^2$$

with $\xi = \mu - \hat{\mu}$, which satisfies

$$\begin{aligned} \frac{dV}{dt} &= \xi^T \dot{\xi} + v^T \dot{v} + \frac{1}{2}e^T \dot{e} \\ &= \xi^T D_z^T \bar{S}_1^T v - \|v\|^2 - v^T \bar{B} D_z e - v^T \bar{S}_1 D_z \xi \\ &\quad + e^T D_z^T \bar{B}^T v \\ &= -\|v\|^2. \end{aligned} \quad (34)$$

From this equality we can conclude that ξ , v , and e are bounded. Moreover, from the definition of e , z is also bounded. Thus, all the states of the autonomous system (28)–(31) are bounded, so one can conclude the convergence of $v(t)$ to zero in view of (34). Furthermore, since $\ddot{v}(t)$ is bounded, then $\dot{v}(t)$ converges also to zero by Barbalat's lemma. By invoking LaSalle's invariance principle, looking at (28) the states e , ξ , and z converge asymptotically to the largest invariance set given by

$$\mathcal{T} \triangleq \{e, z, \xi : \bar{S}_1 D_z \xi + \bar{B} D_z e = \mathbf{0}_{m|\mathcal{V}|\times 1}\} \quad (35)$$

in the compact set

$$\mathcal{Q} \triangleq \{\xi, v, e : \|\xi\|^2 + \|v\|^2 + \frac{1}{2}\|e\|^2 \leq \rho\} \quad (36)$$

with $0 < \rho \leq 2V(0)$. Since $v = \mathbf{0}$ for all points in this invariant set, it follows from (29)–(31) that z , e , and $\hat{\mu}$ are constant in this invariant set. In other words, $z(t) \rightarrow z^*$, $e(t) \rightarrow e^*$, and $\xi(t) \rightarrow \xi^*$ as t goes to infinity, where z^* , e^* , and $\hat{\mu}^*$ are fixed points satisfying (35). Note that by comparing (27) and (29) one can also conclude that $p(t) \rightarrow p^*$ as t goes to infinity. In general, we have that e^* and ξ^* are not zero vectors, therefore, $z^* \notin \mathcal{Z}$. It is also clear that $\|e^*\|^2 \leq 2\rho$, therefore, for a sufficiently small ρ , the resultant (distorted) formation will also be infinitesimally and minimally rigid.

Now we are going to show that $e^*, \xi^* = \mathbf{0}$ for triangles and tetrahedrons. Since triangles and tetrahedrons are derived from complete graphs, the distorted shape when ρ is sufficiently small will also be a triangle or a tetrahedron, i.e., we are excluding nongeneric situations, e.g., collinear or coplanar alignments of

the agents in $\mathbb{R}^2$ or $\mathbb{R}^3$. In the triangular case, we have two possibilities after choosing the estimating agents: Their associated directed graph is cyclic (each agent estimates one mismatch) or acyclic (one agent estimates two mismatches and one of the other two agents estimate the remaining mismatch).

The cyclic case for the estimating agents in the triangle corresponds to the following matrices

$$B = \begin{bmatrix} 1 & 0 & -1 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix} \quad S_1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

and by substituting them into the equilibrium condition in $\mathcal{T}$ we have that

$$\left. \begin{aligned} z_1^* e_1^* - z_3^* e_3^* + z_1^* \xi_1^* &= 0 \\ z_2^* e_2^* - z_1^* e_1^* + z_2^* \xi_2^* &= 0 \\ z_3^* e_3^* - z_2^* e_2^* + z_3^* \xi_3^* &= 0 \end{aligned} \right\}. \quad (37)$$

Since the stationary formation is also a triangle for a sufficiently small ρ , then z_1^* , z_2^* , and z_3^* are linearly independent. Therefore, from (37) we have that $e_3^*, e_1^*, e_2^* = 0$, respectively, and consequently we have that $\xi_1^*, \xi_2^*, \xi_3^* = 0$.

Without loss of generality the acyclic case for the estimating agents in the triangle corresponds to the following matrices

$$B = \begin{bmatrix} -1 & 0 & -1 \\ 1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix} \quad S_1 = \begin{bmatrix} 0 & 0 & 0 \\ 1 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad (38)$$

and by substituting them into the equilibrium condition in $\mathcal{T}$ we have that

$$\left. \begin{aligned} -z_1^* e_1^* - z_3^* e_3^* &= 0 \\ z_2^* e_2^* + z_1^* e_1^* + z_2^* \xi_2^* + z_1^* \xi_1^* &= 0 \\ z_3^* e_3^* - z_2^* e_2^* + z_3^* \xi_3^* &= 0 \end{aligned} \right\}. \quad (39)$$

It is immediate from the first equation in (39) that $e_1^*, e_3^* = 0$ and then from the third equation in (39) we derive that $e_2^*, \xi_3^* = 0$, and hence $\xi_1^*, \xi_2^* = 0$ from the second equation in (39).

For the sake of brevity, we omit the proof for the tetrahedrons, but analogous to the analysis for the triangles, the key idea behind the proof is that the three relative vectors associated to an agent are linearly independent in 3-D. ■

Remark 4.2: The solution proposed in Theorem 4.1 is distributed in the sense that each agent runs its own estimator based on only local information in order to address or solve the *global* problem of a distorted and moving formation.

Remark 4.3: Since the estimating agents are defined by S_1 , by *arbitrarily chosen* we mean that for a given edge in the incidence matrix B , the order of the agents (tail and head) can be chosen arbitrarily.

Remark 4.4: A wide range of shapes can be constructed through piecing together triangles or tetrahedrons. For example, a multiagent deployment of an arbitrary geometric shape in 2-D can be realized by employing a mesh of triangles. If we consider the case when the interaction between different subgroups of triangular formations defines a directed graph (so without mismatches), but each groups' graphs are undirected triangles or tetrahedrons, then one can employ the results of Theorem 4.1.

The use of distributed estimators in Theorem 4.1, except for triangles and tetrahedrons, does not prevent the undesirable effect of having a distortion in the steady-state shape with respect to the desired one. Nevertheless, the error norm $\|e\|$ is bounded by a constant $\sqrt{2\rho} > 0$. Since $\|e\|$ is a combination of all errors in every edge, we cannot use ρ to prescribe a zero asymptotic error for some focus edges or to concentrate the bound only on some edges. This property is relevant if we want to reach a prescribed distance for a high-degree of accuracy for some edges. By exploiting the result in Theorem 4.1 for triangles and tetrahedrons, we can construct a network topology (based on a star topology) that enables us to impose the error bound only on one edge while guaranteeing that the other errors converge to zero. We show this in the following proposition.

Proposition 4.5: Consider the same mismatched formation control system as in Theorem 4.1 with the equilibrium set given by $v = \mathbf{0}_{m|\mathcal{V}|\times 1}$ and $\mathcal{T}$ as in (35). Consider the triangular formation defined by B and S_1 as in (38) for the incidence matrix and the estimating agents, respectively. For any new agent $i, i \geq 4$ added to the formation, if we only link it to the agents 2 and 3, and at the same time we let the agents 2 and 3 to be the estimating agents for the mismatches in the new added links, then for a sufficiently small ρ as in (36)

$$\lim_{t \rightarrow \infty} e_k(t) = 0 \quad \forall k \neq 2 \quad (40)$$

and $|e_2(t)| \leq \sqrt{2\rho}$ for all t .

Proof: Clearly a star topology has been used for the newly added agents, where the center is the triangle formed by agents 1, 2, and 3. Note that the newly added agent $i, i \geq 4$ is forming a triangle with agents 2 and 3. Therefore, as explained in Theorem 4.1, if ρ is sufficiently small, then the resultant distorted formation is also formed by triangles. We prove the claim by induction. First, we derive the equations from $\mathcal{T}$ as in (55) for the proposed star topology with four agents

$$\left. \begin{aligned} -z_1^* e_1^* - z_3^* e_3^* &= 0 \\ z_2^* e_2^* + z_1^* e_1^* - z_4^* e_4 + z_2^* \xi_2^* + z_1^* \xi_1^* + z_4^* \xi_4 &= 0 \\ z_3^* e_3^* - z_2^* e_2^* - z_5^* e_5 + z_3^* \xi_3^* + z_5^* \xi_5 &= 0 \\ z_4^* e_4^* + z_5^* e_5^* &= 0 \end{aligned} \right\}. \quad (41)$$

As explained in the last part of the proof of Theorem 4.1, it is clear that the errors e_1^*, e_3^*, e_4^* , and e_5^* must be zero and $e_2^2 \leq \rho$. For any newly added agent $i \geq 5$, we add a new equation to (41) of the form

$$z_l^* e_l^* + z_{l+1}^* e_{l+1}^* = 0 \quad (42)$$

where l and $l+1$ are the labels of the two newly added edges. Thus, for a sufficiently small ρ we have that z_l^* and z_{l+1}^* are linearly independent so $e_l^*, e_{l+1}^* = 0$. ■

It is possible to be more accurate in the estimation of the mismatches under mild conditions. We in [16] have proposed the following control law for the estimators in order to remove effectively both, the distortion and the steady-state collective motion

$$\hat{u}_k = \kappa(e_k + \mu_k - \hat{\mu}_k) \quad k \in \{1, \dots, |\mathcal{E}|\} \quad (43)$$

where $\kappa \in \mathbb{R}^+$ is a sufficiently high gain to be determined. Consider the following change of coordinates $h_k = e_k + \mu_k -$

$\hat{\mu}_k$ and let $h \in \mathbb{R}^{|\mathcal{E}|}$ be the stacked vector of h_k 's for all $k \in \{1, \dots, |\mathcal{E}|\}$. By defining $S_2 \triangleq B - S_1$, it can be checked that the following autonomous system derived from (28)–(31)

$$\dot{v} = -v - \bar{S}_2 D_z e - \bar{S}_1 D_z h \quad (44)$$

$$\dot{e} = 2D_z \bar{B}^T v \quad (45)$$

$$\dot{h} = 2D_z \bar{B}^T v - \kappa h \quad (46)$$

$$\dot{z} = \bar{B}^T v \quad (47)$$

has an equilibrium at $e = h = \mathbf{0}$, $v = \mathbf{0}$, and $z^* \in \mathcal{Z}$. The linearization of the autonomous system (44)–(47) about such an equilibrium point leads to

$$\begin{bmatrix} \dot{v} \\ \dot{e} \\ \dot{h} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} -\bar{I}_{|\mathcal{V}|} & -\bar{S}_2 D_{z^*} & -\bar{S}_1 D_{z^*} & \mathbf{0} \\ 2D_{z^*} \bar{B}^T & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ 2D_{z^*} \bar{B}^T & \mathbf{0} & -\kappa I_{|\mathcal{E}|} & \mathbf{0} \\ \bar{B}^T & \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{bmatrix} v \\ e \\ h \\ z \end{bmatrix}. \quad (48)$$

From the Jacobian in (48) we know that the stability of the system only depends on v, e , and α and not on z . We consider the following assumption as in [16].

Assumption 4.6: The matrix $F \triangleq \begin{bmatrix} -\bar{I}_{|\mathcal{V}|} & -\bar{S}_2 D_{z^*} \\ 2D_{z^*} \bar{B}^T & \mathbf{0} \end{bmatrix}$ is Hurwitz.

Theorem 4.7: There exists a positive constant κ^* such that the equilibrium corresponding to $\bar{\mu} = \mu, v = \mathbf{0}$, and $e = \mathbf{0}$ (with $z^* \in \mathcal{Z}$) of the autonomous system (28)–(31) with the estimator law (43) is locally exponentially stable under Assumption 4.6 for all $\kappa > \kappa^* > 0$.

Proof: The resulting Jacobian by the linearization of (44)–(47), derived from (28)–(31), evaluated at the desired shape $z^* \in \mathcal{Z}$ is given by (48). Note that the stability of the linear system (48) does not depend on z ; therefore, the (marginal) stability of (48) is given by analyzing the eigenvalues of the first 3×3 blocks, i.e., the dynamics of v, e , and h . Also note that by Assumption 4.6 the first 2×2 blocks, i.e., the matrix F , of the matrix in (48) is Hurwitz. In addition, one can also easily check that the third block, i.e., $-\kappa I_{|\mathcal{E}|}$, of the main diagonal of (48) is negative definite. We consider the following Lyapunov function candidate

$$V(v, e, h) = \begin{bmatrix} v^T & e^T \end{bmatrix} P \begin{bmatrix} v \\ e \end{bmatrix} + \frac{1}{2} \|h\|^2 \quad (49)$$

where P is a positive definite matrix such that $PF^T + FP = -2I$. For brevity, following the same arguments used in the proof of the main theorem in [16], the time derivate of V in a neighborhood of the equilibrium $h = \mathbf{0}, v = \mathbf{0}$, and $e = \mathbf{0}$ (with $z^* \in \mathcal{Z}$) can be given by

$$\frac{dV}{dt} \leq -\|v\|^2 - \|e\|^2 + (m - \kappa) \|h\|^2 \quad (50)$$

where $m \in \mathbb{R}$ comes from the cross-terms that eventually are going to be dominated by $\kappa > \kappa^* = m$. We also refer to the book [28] for more details about the employed technique of requiring F to be Hurwitz and employing the Lyapunov function (49). ■

Remark 4.8: Since $v(t)$ converges exponentially to zero, it follows immediately that $p(t)$ converges exponentially to a fixed point p^* .

Assumption 4.6 is also related to the stability of formation control systems whose graph $\mathbb{G}$ defines a directed sensing topology. In fact, it is straightforward to check that the matrix in Assumption 4.6 is the Jacobian matrix for v and e in a distance-based formation control system (without mismatches) with only directed edges in $\mathbb{G}$, i.e., at the equilibrium (desired shape) the linearized nonlinear system is given by

$$\begin{bmatrix} \dot{v} \\ \dot{e} \end{bmatrix} = F \begin{bmatrix} v \\ e \end{bmatrix}. \quad (51)$$

Therefore, in order to satisfy Assumption 4.6, one has to choose the estimating agents with the same topology as in stable directed rigid formations, e.g., a spanning tree. This selection can be checked in more detail in [16] and [29].

These two presented strategies for the estimators in Theorems 4.1 and 4.7 have advantages and drawbacks: The main advantage of (32) over (43) is that we do not need to compute any gain and that there is a free choice of the estimating agents; on the other hand, (43) guarantees exponential convergence to $\mathcal{Z}$ and a distributed estimation of μ . It is also worth noting that a minor modification in (43) also compensates time varying mismatches as it was studied in [16].

V. MOTION CONTROL OF SECOND-ORDER RIGID FORMATIONS

In this section, we are going to extend the findings in [17] on the formation-motion control from the single-integrator to the double integrator case. In particular, we consider how to design the desired constant velocities ${}^b\omega^*$ and ${}^bv_c^*$ as in Fig. 2 for an infinitesimally and minimally rigid formation, i.e., for $e = \mathbf{0}$. The main feature of this approach is that the desired motion of the shape is designed with respect to O_b but not O_g . Note that the latter is the common approach in the literature [6], [11].

Following a similar strategy as in [17] and [30], we solve the motion control of rigid formation problem for double-integrator agents by employing mismatches as design parameters. More precisely, we assign two motion parameters μ_k and $\tilde{\mu}_k$ to agents i and j in the edge $\mathcal{E}_k = (i, j)$ resulting in the following control law²

$$u = -c_1 v - c_2 \bar{B} D_z e + \bar{A}(\mu, \tilde{\mu})z \quad (52)$$

where $c_1, c_2 \in \mathbb{R}^+$ are gains, $\mu \in \mathbb{R}^{|\mathcal{E}|}$ and $\tilde{\mu} \in \mathbb{R}^{|\mathcal{E}|}$ are the stacked vectors for all μ_k and $\tilde{\mu}_k$ and A is defined by

$$a_{ik} \triangleq \begin{cases} \mu_k, & \text{if } i = \mathcal{E}_k^{\text{tail}} \\ \tilde{\mu}_k, & \text{if } i = \mathcal{E}_k^{\text{head}} \\ 0, & \text{otherwise.} \end{cases} \quad (53)$$

The design of ${}^b\omega^*$ and ${}^bv_c^*$ is done via choosing appropriately the motion parameters μ and $\tilde{\mu}$, in the sense that we allow a desired steady-state collective motion but remove any distortion

²As a comparison, in [17] the proposed controller is of the form of $u = -c_2 \bar{B} D_z e + \bar{A}(\mu, \tilde{\mu})z$.

of the final shape. The design of the motion parameters in A must take into account not only the desired acceleration but also the damping component in (52) (which is different from the single-integrator case considered in [17]).

Let the velocity error

$$e_v = v - \bar{A}_v(\mu, \tilde{\mu})z \quad (54)$$

where $A_v(\mu, \tilde{\mu})$ is designed employing the motion parameters described in [17] directly related to the desired steady-state collective velocity. For the sake of completeness, we briefly describe how to compute μ and $\tilde{\mu}$ in A_v for the prescribed ${}^bv_c^*$ and ${}^b\omega^*$ as in Fig. 2. Since

$$A_v(\mu, \tilde{\mu}){}^bz^* = [\bar{S}_1 D_{b_z^*} \quad \bar{S}_2 D_{b_z^*}] \begin{bmatrix} \mu \\ \tilde{\mu} \end{bmatrix} = T({}^bz^*) \begin{bmatrix} \mu \\ \tilde{\mu} \end{bmatrix} \quad (55)$$

defines the steady-state velocity in the body frame, one can derive the following two conditions

$$\bar{B}^T \bar{T}({}^bz^*) \begin{bmatrix} \mu \\ \tilde{\mu} \end{bmatrix} = \mathbf{0} \quad (56)$$

$$D_{b_z} \bar{B}^T \bar{T}({}^bz^*) \begin{bmatrix} \mu \\ \tilde{\mu} \end{bmatrix} = \mathbf{0} \quad (57)$$

where (56) stands for translations and (57) for rotations and translations, i.e., we set $\frac{dz_k^*(t)}{dt} = 0$ and $\frac{d\|z_k^*(t)\|}{dt} = 0$ for all $k \in \{1, \dots, |\mathcal{E}|\}$ in (56) and (57), respectively. Let us split $\mu = \mu_v + \mu_\omega$ and $\tilde{\mu} = \tilde{\mu}_v + \tilde{\mu}_\omega$. In order to compute the distributed motion parameters $\mu_v, \tilde{\mu}_v$ for the translational velocity ${}^bv_c^*$, we eliminate the components of μ and $\tilde{\mu}$ that are not responsible for any motion by projecting the kernel of $\bar{B}^T T({}^bz^*)$ onto the orthogonal space of the kernel of $T({}^bz^*)$, namely

$$\begin{bmatrix} \mu_v \\ \tilde{\mu}_v \end{bmatrix} \in \hat{\mathcal{U}} \triangleq P_{\text{Ker}\{T({}^bz^*)\}^\perp} \left\{ \text{Ker}\{\bar{B}^T T({}^bz^*)\} \right\} \quad (58)$$

where the operator $P_{\mathcal{X}}$ stands for the projection over the space $\mathcal{X}$. In a similar way, we need to remove the components responsible for the translational motion in the null space of the matrix in (57). Therefore, the computation of the distributed motion parameters $\mu_\omega, \tilde{\mu}_\omega$ for the rotational motion ${}^b\omega^*$ of the desired shape is obtained from (57) and (58) as

$$\begin{bmatrix} \mu_\omega \\ \tilde{\mu}_\omega \end{bmatrix} \in \hat{\mathcal{W}} \triangleq P_{\hat{\mathcal{U}}^\perp} \left\{ \text{Ker}\{D_{b_z^*}^T \bar{B}^T T({}^bz^*)\} \right\}. \quad (59)$$

When the velocity error e_v is zero and we are at the desired shape $z^*(t) \in \mathcal{Z}$ with the desired velocities in $v^*(t)$, then from (54) we have that

$$v^*(t) = \bar{A}_v z^*(t) \quad (60)$$

$$\begin{aligned} \dot{v}^*(t) &= \bar{A}_v \dot{z}^*(t) = \bar{A}_v \bar{B}^T v^*(t) = \bar{A}_v \bar{B}^T \bar{A}_v z^*(t) \\ &= \bar{A}_a z^*(t). \end{aligned} \quad (61)$$

Note that the desired parameters in $A_a(\mu, \tilde{\mu})$ correspond to the desired acceleration of the agents at the desired shape $\mathcal{Z}$. With this knowledge at hand, we can design the needed motion parameters for A in the control law in (52) as

$$A(\mu, \tilde{\mu}) = c_1 A_v(\mu, \tilde{\mu}) + A_a(\mu, \tilde{\mu}) \quad (62)$$

since for $e_v = \mathbf{0}_{m|\mathcal{V}|\times 1}$ and $e = \mathbf{0}_{|\mathcal{E}|\times 1}$ the control law (52) becomes

$$u = \bar{A}_a(\mu, \tilde{\mu})z^*(t). \quad (63)$$

Note that $A(\mu, \tilde{\mu})$ can be computed directly from the motion parameters for the desired velocity as in the first-order case. Therefore, there is no need of designing desired accelerations, which can be a more tedious task. We show in the following theorem that the desired collective-motion for the desired formation is stable for at least sufficiently small speeds.

Theorem 5.1: There exist constants $\rho, \rho_\mu, \epsilon, c_1, c_2 > 0$ for system (3) with control law (52), $A(\mu, \tilde{\mu})$ as in (53) and with a given desired infinitesimally and minimally rigid shape $\mathcal{Z}$, such that if $[\frac{\mu}{\tilde{\mu}}] \in \mathcal{M} \triangleq \{\mu, \tilde{\mu} : \|\frac{\mu}{\tilde{\mu}}\| \leq \rho_\mu\}$, then the origin of the error dynamical system $e_v = \mathbf{0}$ and $e = \mathbf{0}$ corresponding to $z^*(t) \in \mathcal{Z}$ is exponentially stable in the compact set $\mathcal{Q} \triangleq \{e, e_v : \frac{\epsilon c_1 + c_2}{4}\|e\|^2 + \frac{1}{2}\|e_v\|^2 \leq \rho\}$. In particular, the steady-state shape is the same as the desired one and the steady-state collective motion of the formation corresponds to $v^*(t) = \bar{A}_v z^*(t)$.

Proof: First we rewrite the control law (52) employing (54) and (53) as

$$u = -c_1 e_v - c_2 \bar{B} D z e + \bar{A}_a z. \quad (64)$$

Consider the following candidate Lyapunov function

$$V = \frac{\epsilon c_1 + c_2}{4}\|e\|^2 + \frac{1}{2}\|e_v\|^2 + \epsilon e_v^T \bar{B} D z e \quad (65)$$

where V is positive definite in a neighborhood about $e = \mathbf{0}$ and $e_v = \mathbf{0}$ for some sufficiently small $\epsilon \in \mathbb{R}^+$ in the compact set $\mathcal{Q}$ with $e = \mathbf{0}$ corresponding to $z \in \mathcal{Z}$. Note that even without knowing c_1 and c_2 yet, one can safely compute ϵ by assuming $c_1 = 0$ and $c_2 = c_2^*$ for an arbitrary $c_2^* \in \mathbb{R}^+$. Then, later we restrict the choosing of c_1 and c_2 to be bigger than 0 and c_2^* , respectively, since by this choice one does not change the positive semidefinite nature of (65) for the calculated ϵ for $c_1 = 0$ and $c_2 = c_2^*$.

The time derivative of (65) is given by

$$\begin{aligned} \frac{dV}{dt} &= \frac{1}{2}(\epsilon c_1 + c_2)e^T \dot{e} + e_v^T \dot{e}_v + \epsilon e_v^T \bar{B} D z \dot{e} + \epsilon e^T D_z^T \bar{B}^T \dot{e}_v \\ &\quad + \epsilon e_v^T \bar{B} D_{(\bar{B}^T v)} e \\ &= (\epsilon c_1 + c_2)e^T D_z^T \bar{B}^T (e_v + \bar{A}_v z) - c_1 \|e_v\|^2 \\ &\quad - c_2 e_v^T \bar{B} D z e \\ &\quad + e_v^T \bar{A}_v \bar{B}^T \bar{A}_v z - e_v^T \bar{A}_v \bar{B}^T \bar{A}_v z - e_v^T \bar{A}_v \bar{B}^T e_v \\ &\quad + 2\epsilon e_v^T \bar{B} D z D_z^T \bar{B}^T v - c_1 \epsilon e^T D_z^T \bar{B}^T e_v \\ &\quad - c_2 \epsilon e^T D_z^T \bar{B}^T \bar{B} D z e \\ &\quad + \epsilon e^T D_z^T \bar{B}^T \bar{A}_v \bar{B}^T \bar{A}_v z - \epsilon e^T D_z^T \bar{B}^T \bar{A}_v \bar{B}^T \bar{A}_v z \\ &\quad - \epsilon e^T D_z^T \bar{B}^T \bar{A}_v \bar{B}^T e_v + \epsilon e_v^T \bar{B} D_{(\bar{B}^T v)} e \end{aligned}$$

$$\begin{aligned} &= (\epsilon c_1 + c_2)e^T \underbrace{D_z^T \bar{B}^T \bar{A}_v z}_{f_1(e, \mu, \tilde{\mu})} - c_1 \|e_v\|^2 - e_v^T \underbrace{\bar{A}_v \bar{B}^T}_{f_2(\mu, \tilde{\mu})} e_v \\ &\quad + 2\epsilon e_v^T \underbrace{\bar{B} D z D_z^T \bar{B}^T}_{f_3(z)} e_v + 2\epsilon e_v^T \underbrace{\bar{B} D z D_z^T \bar{B}^T \bar{A}_v z}_{f_4(\mu, \tilde{\mu}, z, e)} \\ &\quad - c_2 \epsilon e^T \underbrace{D_z^T \bar{B}^T \bar{B} D z e}_{f_5(e)} - \epsilon e^T \underbrace{D_z^T \bar{B}^T \bar{A}_v \bar{B}^T}_{f_6(\mu, \tilde{\mu}, z)} e_v \\ &\quad + \epsilon e_v^T \underbrace{\bar{B} D_{(\bar{B}^T v)}}_{f_7(v)} e. \end{aligned} \quad (66)$$

Since all the $f_i, i \in \{1, \dots, 7\}$ are locally Lipschitz functions in the compact sets $\mathcal{Q}$ and $\mathcal{M}$ and by using Young's inequality to every cross-term in (66), we can bound $\dot{V}$ as follows

$$\begin{aligned} \frac{dV}{dt} &\leq \left(c_2 \left(M_1(\mu, \tilde{\mu}) - \epsilon \lambda_5 \right) + \epsilon c_1 M_1(\mu, \tilde{\mu}) + \frac{3}{2} \right) \|e\|^2 \\ &\quad + \left(-c_1 + M_2(\mu, \tilde{\mu}) \right) \|e_v\|^2 \\ &\quad + \epsilon^2 \left(\frac{2\lambda_3}{\epsilon} + M_4(\mu, \tilde{\mu}, z) + M_6(\mu, \tilde{\mu}, z) + M_7 \right) \|e_v\|^2 \end{aligned} \quad (67)$$

where M_1 and M_4 are related to the Lipschitz constant of f_1 and f_4 in the compact set $\mathcal{Q}$ given μ and $\tilde{\mu}$, M_2 is the induced 2-norm of f_2 given μ and $\tilde{\mu}$, M_6 is the squared induced 2-norm of f_4 in the compact set $\mathcal{Q}$ given μ and $\tilde{\mu}$, and finally M_7 is the maximum squared induced 2-norm for f_7 in $\mathcal{Q}$ as well. We also have that λ_3 is the maximum eigenvalue of f_3 and λ_5 is the minimum eigenvalue of f_5 in the compact set $\mathcal{Q}$. First, we note that for a sufficiently small ρ , $\lambda_5 > 0$ by the same argument of having a desired infinitesimally and minimally rigid formation as in Lemma 3.2. The time derivative (67) can be made negative as a result of the following steps:

- 1) Choose a sufficiently small ρ_μ in $\mathcal{M}$ such that $M_1(\mu, \tilde{\mu}) - \epsilon \lambda_5 < 0$, i.e., downscale if necessary μ and $\tilde{\mu}$ by the same factor.
- 2) Compute M_2 for the given $\mu, \tilde{\mu}$.
- 3) Compute M_4 and M_6 for the given $\mu, \tilde{\mu}$ in the compact set $\mathcal{Q}$.
- 4) Compute M_7 considering all the v such that $\|e_v\|^2 \leq \rho$.
- 5) Choose c_1 such that the second bracket in (67) is negative.
- 6) Given c_1 choose $c_2 \geq c_2^*$ (employed for the calculation of ϵ) such that the first bracket in (67) is negative.

This guarantees the local exponential convergence of $e(t)$ and $e_v(t)$ to their origins, hence $z(t) \rightarrow z^*(t) \in \mathcal{Z}$, $v(t) \rightarrow \bar{A}_v z^*(t)$ and the stacked acceleration of the agents $a(t) \rightarrow \bar{A}_a z^*(t)$ as t goes to infinity. ■

Remark 5.2: The limitation given by ρ_μ is exclusively related to the desired speed of the agents [17] and it does not restrict in any other way the desired collective motion for the formation. Therefore, once the motion parameters are given, for asserting the exponential stability of the system, one only has to downscale them if necessary. This (conservative) downscale has an intuitive physical explanation related to the condition of

requiring $\lambda_5 > 0$ in Theorem 5.1, e.g., the agents cannot be in a collinear configuration at any moment. In order to avoid such configurations where λ_5 is zero we need $e \in \mathcal{Q}$, i.e., for arbitrary velocities and positions of the agents such that $e, e_v \in \mathcal{Q}$, the third acceleration term in (64) given by the motion parameters μ and $\tilde{\mu}$ must be small enough in order to avoid the possibility of pushing the agents to become collinear. Note that when the agents start close to the desired shape and have low velocity, the gradient terms in (64) will not push the agents to such a configuration but to the desired shape. Nevertheless, imposing $\lambda_5 > 0$ for all time is a very conservative condition and we have verified in simulation that indeed it is not a necessary condition.

Remark 5.3: For $\mu, \tilde{\mu} = \mathbf{0}$ we have that $M_1, M_2, M_3, M_4, M_6 = 0$. Then employing (65) and applying differently Young's inequalities in (66) one can prove that for $c_1, c_2 = 1$ the dissipative Hamiltonian system (6) is exponentially stable for a sufficiently small ϵ .

Remark 5.4: For desired constant drifts in triangular and tetrahedron formations, it can be checked from [17] that $M_1 = 0$. Therefore, there is no restriction in the speed for such particular cases. In particular, one can use the Lyapunov function (65) with $\epsilon = 0$. It turns out that the formation with the proposed motion-shape controller is asymptotically stable for any $c_2 > 0$ for $c_1 > \|\bar{A}_v(\mu, \tilde{\mu})\bar{B}^T\|^2$.

Remark 5.5: For a desired rotation about the centroid of an equilateral triangle, it can be checked from [17] that in addition to $M_1 = 0$ we have that $e_v^T f_2(\mu, \tilde{\mu})e_v = 0$ since f_2 is skew symmetric. Therefore, by using (65) with $\epsilon = 0$ one can prove the asymptotic stability of the origin of e_v and e for any $c_1, c_2 > 0$.

Remark 5.6: We recall the mismatched case in Section III-B. So far, we can conclude that the upper bound for the distortion and speed of the resulting formation depends on the steady state of the formed geometrical shape. This can be seen by looking at the third term on the right-hand side of (52) by just taking $\tilde{\mu} = \mathbf{0}$. On the other hand, there is a direct relation between a formation containing mismatches with a formation containing motion parameters by checking the two cases in (16) and (64). In the latter case, we are able to calculate the steady state of both shape and velocity. In the former (mismatched) case, we refer to the results in [22] in order to check the approximated resultant motion. As a first step, the distortion in the mismatched case can be approached by comparing how far the mismatches are from the ones calculated employing (58), (59), and (53), where no distortion occurs.

The result in Theorem 5.1 allows one to design the desired velocity for the given formation with respect to O_b as in Fig. 2. This result extends to the applications proposed in [17] by using distributed motion parameters, such as steering an infinitesimally and minimally rigid formation by controlling the heading of the formation with respect to O_g , and for the tracking and enclosing of a target.

VI. SIMULATIONS

In this section, we validate the results in Theorems 4.1, 4.7, and 5.1 with numerical simulations.

Fig. 3. Numerical simulation of a team of four agents with mismatches in their prescribed distances. We employ the estimator proposed in Theorem 4.1. The final positions of the agents are marked with dots, respectively, and the red, green, blue, and black colors correspond to the agents 1, 2, 3, and 4, respectively. The effectiveness of the estimator is shown in (b) and (c), where all the agents' speed and errors [as defined in (8)] converge effectively to zero. The plot (d) shows how the six elements of the estimator state $\hat{\mu}$ converge to the actual μ (shown in black dashed lines).

We first start validating Theorem 4.1 for a regular tetrahedron formation, with side length equal to 70 units, whose associated incidence matrix is given by

$$B = \begin{bmatrix} -1 & 0 & -1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 & 0 & 1 \\ 0 & -1 & 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & -1 & -1 & -1 \end{bmatrix}. \quad (68)$$

We then randomly generate the following vector of mismatches μ for each edge $\mathcal{E}_k$

$$\mu = [12.14 \quad -41.12 \quad -16.64 \quad -5.91 \quad 0.45 \quad 18.41]^T. \quad (69)$$

We randomly spread the four agents within an area of 100 cubic units and with random initial velocities but with speeds smaller than 2 units per second. We apply the control law as in (28) with the estimator dynamics (32). We remark that with this setup, one can choose arbitrarily the estimating agents, i.e., how one chooses B for defining the (mismatched) tetrahedron formation does not matter. The results are shown in Fig. 3.

We now have a team of six agents whose prescribed shape is a regular hexagon, with side length equal to 50 units, whose incidence matrix is given by

$$B = \begin{bmatrix} 1 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & -1 & -1 & 1 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 & 1 & 1 & 0 \\ 0 & 0 & 0 & 0 & -1 & -1 & -1 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & -1 \end{bmatrix}. \quad (70)$$

Fig. 4. Regular hexagon formation where the tails of the arrows indicate the corresponding estimating agents. Note that this configuration does not contain any cycles; and therefore, Assumption 4.6 is satisfied.

Fig. 5. Numerical simulation of a team of six agents for forming a hexagon but with mismatches in their prescribed distances. We employ the estimator proposed in Theorem 4.7. The final positions of the agents are marked with dots, respectively, and the red, green, blue, black, magenta, and cyan colors correspond to the agents 1, 2, 3, 4, 5, and 6, respectively. The effectiveness of the estimator is shown in (b) and (c), where all the agents' speed and errors [as defined in (8)] converge effectively to zero. The plot (d) shows how the nine elements of the estimator state $\hat{\mu}$ converge to the actual μ (shown in black dashed lines).

and we add the following arbitrary vector of mismatches

$$\mu = 0.1 \begin{bmatrix} -0.43 \\ 7.09 \\ 0.08 \\ -1.19 \\ -5.55 \\ -0.574 \\ 7.33 \\ 1.85 \\ -1.05 \end{bmatrix}. \quad (71)$$

We use the results in Theorem 4.7 in order to eliminate the undesired steady-state motion and distortion in the desired shape. We first notice that the estimating agents defined by S_1 derived from B are not defining any cycles as it can be checked in Fig. 4. Therefore, the topology for the estimating agents makes Assumption 4.6 to be satisfied. Since the equilibrium set for the shape is given by $\mathcal{D}$ and not by $\mathcal{Z}$, in order to have a hexagon as a final shape, one restricts the initial positions of the agents to be close to the desired shape and with small initial velocities. We consider the gain $\kappa = 1$ for (43), but noting that this value

Fig. 6. Numerical simulation of a team of four agents travelling in a tetrahedron formation. We employ the results from Theorem 5.1. In the first plot the agents 1, 2, 3, and 4 are marked with the red, green, blue, and black colors, respectively. The crosses indicate the initial positions. The black agent *on top* of the tetrahedron follows a linear velocity, whereas the other three agents follow the same velocity and in addition they are spinning about the centroid of the base of the tetrahedron. We show in plots (a) and (b), the evolution of the inter-agent distances and the speeds of the agents, converging to the desired ones (dashed lines).

is smaller than the conservative one that can be derived from Theorem 4.7. The results are shown in Fig. 5.

In order to validate the results of Theorem 5.1, we consider the previous four agents from the first experiment but with a regular tetrahedron of side length equal to 25 units as a desired shape. The chosen incidence matrix is the same as (68). The desired motion of the tetrahedron is given in Fig. 2 but with $b_{v_c}^*$ being parallel to b_{ω}^* , i.e., the agent on the *top* of the tetrahedron is following a linear velocity perpendicular to the base, the other three agents follow the same linear velocity, and in addition these three agents also make spinning about the centroid of the base. In order to have such a motion, the distributed motion parameters for A_v as in (54) are given by

$$\begin{cases} \mu_v = s_v [1 & 1 & 1 & -3 & -3 & -3]^T \\ \tilde{\mu}_v = s_v [-1 & -1 & -1 & -1 & -1 & -1]^T \\ \mu_\omega = s_\omega [1 & 1 & 1 & 0 & 0 & 0]^T \\ \tilde{\mu}_\omega = s_\omega [1 & 1 & 1 & 0 & 0 & 0]^T \end{cases} \quad (72)$$

where we set $s_v = 0.15$ and $s_\omega = 0.25$, i.e., we regulate the speeds of $b_{v_c}^*$ and b_{ω}^* such that the speed of the agent 4 is $0.15||z_4^* + z_5^* + z_6^*|| = 9.184$ units per second. Similar calculations can be done for the other three agents in order to derive that their stationary speed will be 11.113 units per second. We randomly spread the four agents within an area of 50 cubic units and with random initial velocities with the initial speeds smaller than 2 units per second. We apply the control law (52) to system (3), constructing A with (72) as in (53) and with control gains $c_1 = 1$ and $c_2 = 1$, which are smaller than the conservative ones

derived from Theorem 5.1, showing the conservative nature of the result of the theorem. The numerical results are shown in Fig. 6.

VII. CONCLUSION

In this paper, we have analyzed the effects of having a distance-based controller for rigid formations and second-order agents with the presence of mismatches in their desired inter-agent distances. These effects are a stationary distorted shape with respect to the desired one and an undesired collective motion of the formation. It turns out that both first-order and second-order agents share precisely the same behavior for the undesired collective motion. We have extended the estimator based solution proposed in [16] to remove the effects of the mismatches to second-order agents. We have also proposed another estimator with fewer requirements although it only eliminates all the undesired effects for both triangles and tetrahedrons. For the rest of shapes, the new estimator is only effective for removing the undesired state-state collective motion. Nevertheless, a bound on the distortion of the steady-state shape with respect to the desired is given. We have further extended the results from [17] of employing distributed motion parameters in order to control the motion of a desired rigid shape to the second-order agents case. Consequently, it opens possibilities to apply this method directly to actual systems governed by Newtonian dynamics such as quadrotors or marine vessels as it has been shown in [31]. We are currently working on extending the recent results for *flexible* formations with mismatches [32], [33] to second-order agents as well.

REFERENCES

- [1] K. Cesare, R. Skeele, S.-H. Yoo, Y. Zhang, and G. Hollinger, "Multi-UAV exploration with limited communication and battery," in *Proc. 2015 IEEE Int. Conf. Robot. Autom.*, May 2015, pp. 2230–2235.
- [2] W. Burgard, M. Moors, D. Fox, R. Simmons, and S. Thrun, "Collaborative multi-robot exploration," in *Proc. IEEE Int. Conf. Robot. Autom.*, vol. 1, 2000, pp. 476–481.
- [3] S. Tsugawa, S. Kato, and K. Aoki, "An automated truck platoon for energy saving," in *Proc. 2011 IEEE/RSJ Int. Conf. Intell. Robot. Syst.*, 2011, pp. 4109–4114.
- [4] J. Guo, G. Yan, and Z. Lin, "Local control strategy for moving-target-enclosing under dynamically changing network topology," *Syst. Control Lett.*, vol. 59, no. 10, pp. 654–661, 2010.
- [5] S. Hara, T.-H. Kim, Y. Hori, and K. Tae, "Distributed formation control for target-enclosing operations based on a cyclic pursuit strategy," in *Proc. 17th IFAC World Congr.*, 2008, pp. 6602–6607.
- [6] H. Bai, M. Arcak, and J. Wen, *Cooperative Control Design: A Systematic, Passivity-Based Approach*. New York, NY, USA: Springer-Verlag, 2011.
- [7] R. Olfati-Saber and R. M. Murray, "Graph rigidity and distributed formation stabilization of multi-vehicle systems," in *Proc. 41st IEEE Conf. Decis. Control*, 2002, pp. 2965–2971.
- [8] L. Krick, M. E. Broucke, and B. A. Francis, "Stabilization of infinitesimally rigid formations of multi-robot networks," *Int. J. Control*, vol. 82, pp. 423–439, 2009.
- [9] C. Yu, B. D. O. Anderson, S. Dasgupta, and B. Fidan, "Control of minimally persistent formations in the plane," *SIAM J. Control Optim.*, vol. 48, pp. 206–233, 2009.
- [10] M. Cao, C. Yu, and B. D. O. Anderson, "Formation control using range-only measurements," *Automatica*, vol. 47, pp. 776–781, 2011.
- [11] K.-K. Oh, M.-C. Park, and H.-S. Ahn, "A survey of multi-agent formation control," *Automatica*, vol. 53, pp. 424–440, 2015.
- [12] Z. Sun, Q. Liu, C. Yu, and B. D. O. Anderson, "Generalized controllers for rigid formation stabilization with application to event-based controller design," in *Proc. Eur. Control Conf.*, 2015, pp. 217–222.
- [13] Z. Sun and B. Anderson, "Rigid formation control systems modelled by double integrators: System dynamics and convergence analysis," in *Proc. 2015 5th Aust. Control Conf.*, Nov. 2015, pp. 241–246.
- [14] S. Mou, M.-A. Belabbas, A. S. Morse, Z. Sun, and B. D. O. Anderson, "Undirected rigid formations are problematic," *IEEE Trans. Autom. Control*, vol. 61, no. 10, pp. 2821–2836, Oct. 2016.
- [15] U. Helmke, S. Mou, Z. Sun, and B. D. O. Anderson, "Geometrical methods for mismatched formation control," in *Proc. 2014 IEEE 53rd Annu. Conf. Decis. Control*, 2014, pp. 1341–1346.
- [16] H. G. de Marina, M. Cao, and B. Jayawardhana, "Controlling rigid formations of mobile agents under inconsistent measurements," *IEEE Trans. Robot.*, vol. 31, no. 1, pp. 31–39, Feb. 2015.
- [17] H. G. de Marina, B. Jayawardhana, and M. Cao, "Distributed rotational and translational maneuvering of rigid formations and their applications," *IEEE Trans. Robot.*, vol. 32, no. 3, pp. 684–697, Jun. 2016.
- [18] D. Mellinger, N. Michael, and V. Kumar, "Trajectory generation and control for precise aggressive maneuvers with quadrotors," *Int. J. Robot. Res.*, vol. 31, no. 5, pp. 664–674, 2012.
- [19] E. J. Smeur, G. C. de Croon, and Q. Chu, "Gust disturbance alleviation with incremental nonlinear dynamic inversion," in *Proc. 2016 IEEE/RSJ Int. Conf. Intell. Robot. Syst.*, 2016, pp. 5626–5631.
- [20] T. I. Fossen, *Marine Control Systems: Guidance, Navigation and Control of Ships, Rigs and Underwater Vehicles*. Tiller, Norway: Marine Cybernetics AS, 2002.
- [21] M. Deghat, B. Anderson, and Z. Lin, "Combined flocking and distance-based shape control of multi-agent formations," *IEEE Trans. Autom. Control*, vol. 61, no. 7, pp. 1824–1837, Jul. 2016.
- [22] Z. Sun, S. Mou, B. Anderson, and A. Morse, "Formation movements in minimally rigid formation control with mismatched mutual distances," in *Proc. 2014 IEEE 53rd Annu. Conf. Decis. Control*, Dec. 2014, pp. 6161–6166.
- [23] B. D. O. Anderson, C. Yu, B. Fidan, and J. Hendrickx, "Rigid graph control architectures for autonomous formations," *IEEE Control Syst. Mag.*, vol. 28, no. 6, pp. 48–63, Dec. 2008.
- [24] Henneberg, "Die graphische statik der starren systeme," Leipzig, Germany: BG Teubner, 1911.
- [25] A. van der Schaft, "Port-Hamiltonian systems: An introductory survey," in *Proc. Int. Congr. Mathematicians Vol. III: Invited Lectures*. Madrid, Spain: European Mathematical Society Publishing House, 2006, pp. 1339–1365.
- [26] K. Oh and H. Ahn, "Distance-based undirected formation of single-integrator and double-integrator modeled agents in n-dimensional space," *Int. J. Robust Nonlinear Control*, vol. 12, pp. 1809–1820, 2014.
- [27] H. K. Khalil and J. Grizzle, *Nonlinear Systems*, vol. 3. Englewood Cliffs, NJ, USA: Prentice-Hall, 1996.
- [28] A. Isidori, "Nonlinear control systems," Berlin, Germany: Springer-Verlag, 2013.
- [29] J. M. Hendrickx, B. Fidan, C. Yu, B. D. O. Anderson, and V. D. Blondel, "Formation reorganization by primitive operations on directed graphs," *IEEE Trans. Autom. Control*, vol. 53, no. 4, pp. 968–979, May 2008.
- [30] H. G. de Marina, B. Jayawardhana, and M. Cao, "Distributed scaling control of rigid formations," in *Proc. 2016 IEEE 55th Ann. Conf. Decis. Control*, Dec. 2016, pp. 5140–5145.
- [31] H. G. de Marina, "Distributed formation control for autonomous robots," Ph.D. dissertation, University of Groningen, 2016.
- [32] H. G. de Marina, B. Jayawardhana, and M. Cao, "Distributed algorithm for controlling scale-free polygonal formations," in *Proc. 20th IFAC World Congr.*, 2017.
- [33] H. G. de Marina, Z. Sun, M. Cao, and B. D. O. Anderson, "Controlling a triangular flexible formation of autonomous agents," in *Proc. 20th IFAC World Congr.*, 2017.

Hector Garcia de Marina (M'16) received the M.Sc. degree in electronics engineering from Complutense University of Madrid, Madrid, Spain, in 2008 and the M.Sc. degree in control engineering from the University of Alcalá de Henares, Alcalá de Henares, Spain, in 2011.

He is currently a Postdoctoral Research Associate with the Ecole Nationale de l'Aviation Civile, Toulouse, France. His research interests include formation control and navigation for autonomous robots, and drones in particular.

Bayu Jayawardhana (SM'13) received the B.Sc. degree in electrical and electronics engineering from the Institut Teknologi Bandung, Bandung, Indonesia, in 2000, the M.Eng. degree in electrical and electronics engineering from the Nanyang Technological University, Singapore, in 2003, and the Ph.D. degree in electrical and electronics engineering from Imperial College London, London, U.K., in 2006.

He is currently an Associate Professor in the Faculty of Mathematics and Natural Sciences, University of Groningen, Groningen, The Netherlands. He was with Bath University, Bath, U.K., and with Manchester Interdisciplinary Biocentre, University of Manchester, Manchester, U.K. His research interests include the analysis of nonlinear systems, systems with hysteresis, mechatronics, systems, and synthetic biology.

Prof. Jayawardhana is a Subject Editor of the *International Journal of Robust and Nonlinear Control*, an Associate Editor of the *European Journal of Control*, and a member of the Conference Editorial Board of the IEEE Control Systems Society.

Ming Cao (SM'16) received the Bachelor's degree in 1999 and the Master's degree in 2002 from Tsinghua University, Beijing, China, and the Ph.D. degree in 2007 from Yale University, New Haven, CT, USA, all in electrical engineering.

He is currently a Professor of systems and control with the Engineering and Technology Institute, University of Groningen, Groningen, the Netherlands, where he started as a tenure-track Assistant Professor in 2008. From September 2007 to August 2008, he was a Postdoctoral Research Associate in the Department of Mechanical and Aerospace Engineering at Princeton University, Princeton, NJ, USA. He worked as a research intern during the summer of 2006 with the Department of Mathematical Sciences, IBM T. J. Watson Research Center, NY, USA. His main research interests include autonomous agents and multiagent systems, mobile sensor networks, and complex networks.

Dr. Cao received the Manfred Thoma medal from the International Federation of Automatic Control (IFAC) in 2017 and the European Control Award from the European Control Association in 2016. He is an Associate Editor of the IEEE TRANSACTIONS ON AUTOMATIC CONTROL, the IEEE TRANSACTIONS ON CIRCUITS AND SYSTEMS, and *Systems and Control Letters*, and for the Conference Editorial Board of the IEEE Control Systems Society. He is also a member of the IFAC Technical Committee on Networked Systems.